

User Guide
for
Design Advisor
Version 4

By

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Executive Summary

Making a material selection decision for an automotive component is complicated by several factors. First, it is generally recognized that such decisions should be based on the effect on the overall vehicle system rather than considering *only* effects of the component. Second, the decision criteria (what determines ‘best’) are multiple attributes. These attributes address such questions as: How is the vehicle system mass affected by the material selected: How is the vehicle system cost impacted: How will fuel economy be impacted? How will environmental stressors be impacted over the life cycle of the vehicle system? Since these criteria are not easily combined as a single objective number, the decision maker must be presented with several attributes (mass, cost, greenhouse gas) so any trade-offs between attributes may be recognized.

The objective of the *Design Advisor* software is to provide the decision-maker with a tool to evaluate these component material selection decisions at a vehicle system level, and using multiple attributes of vehicle mass, cost, and life cycle stress on the environment. Because these material selection decisions are often made very early in the vehicle design cycle, the *Design Advisor* is configured to operate in that context. First, only information which would be available during the vehicle planning stage is required as input. Second, to support quick decision making during meetings, Microsoft Excel was the chosen application because of its wide availability on laptops. Third, the interface is intended to be intuitive and visual as the assumed decision maker may be other than an analyst. Finally, because of the approximate nature of input data, a sensitivity analysis is included to allow varying the input values to evaluate the robustness of the estimates.

Primary updates for Version 4 (version shown in brackets after each item) include:

- 1) Functional and usability changes in response to comments from members and other users [version 4.0]
- 2) Updating mass influence coefficients with new data from EDAG [version 4.1]
- 3) Updating energy demand and Fuel Reduction Values for the corrected US schedule from fka [v4.1]
- 4) Updating benchmark charts with new data from EDAG [version 4.1]
- 5) Updating benchmark equations from EDAG [version 4.1]
- 6) Updating material list in Bill of Materials consistent with UCSB v4 [version 4.1]
- 7) Change material production GHG to include prompt scrap recycling consistent with UCSB v4 [v4.1]
- 8) Changing any parameters to be consistent with UCSB v4 [version 4.1]

Acknowledgements

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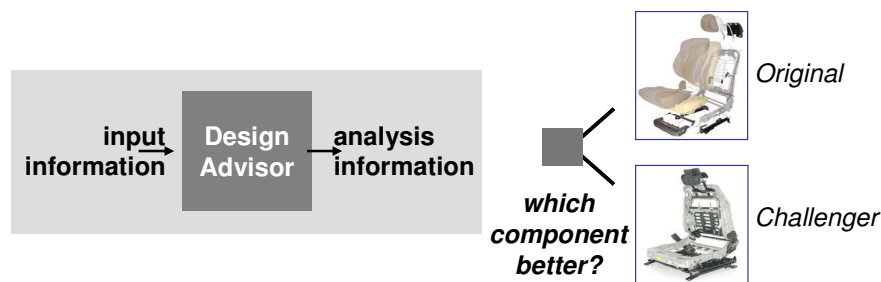
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1- Introduction

Making a material selection decision for an automotive component is complicated by several factors. First, it is generally recognized that such decisions should be based on the effect on the overall vehicle system rather than considering *only* how the component is affected. Second, the decision is based on multiple attributes. These attributes include such questions as: How is the vehicle system mass affected by the material selected; How is the vehicle system cost impacted; How will environmental stressors be impacted over the life cycle of the vehicle system? Often these attributes point to a different preference and the decision maker must understand any trade-offs between attributes.

This user guide describes a software tool called the *Design Advisor*. The purpose of the *Design Advisor* is to provide rapid, quantitative evaluation for a material selection decision for two alternative components. This evaluation is done at a vehicle system level, and considers mass, cost, and life cycle greenhouse gas.



Example selection context for Design Advisor

1.1 Description of the model- In the *Design Advisor*, the user is stepped through the process of building two vehicles; a nominal vehicle with the original component, and a resized vehicle with the competitor component. The performance of these two vehicles is then compared using several metrics.

Before describing the model, a few definitions are needed.

Component –The assembly under study.

Part–The part within the component whose material is varied. This may be a weldment of several pieces. The part is the primary focus of the analysis.

Original component/part–The component of the original material and design concept.

Competitor component/part –An alternative to the original. The decision on whether to use the original or competitor component is being made.

Nominal vehicle – The vehicle as defined by the user and having the original component.

Resized vehicle – The nominal vehicle with the competitor component substituted for the original component, and with subsystems resized due to differences in mass between the original and competitor components.

Primary changes –Changes in mass/cost/CO₂ between the original and competitor *components*.

Subsystem resizing changes –Changes in mass/cost/CO₂ between the nominal vehicle with original component and the resized vehicle with the competitor component. These are also called Secondary changes.

The overall calculation method is a five step sequence.

Step 1a—Define a nominal vehicle with the original component. A nominal vehicle is defined based on vehicle type (Sedan/Hatchback or SUV), the foot print area, the powertrain type, and the number of passengers and cargo. Based on benchmark data, vehicle mass and subsystem mass are determined for a typical vehicle of that size and class.

Step 1b- A powertrain is sized for the nominal vehicle by specifying fuel consumption, fuel type, driving schedule, and life time range.

Step 2a- The original and competitor component technology is input. This includes mass for the component and part, the part material, and the shaping process. It is assumed this information is available from a previous study of the component design concepts.

Step 2b- The component is scaled to fit in this nominal vehicle. Benchmark data is used to scale the component mass from the original study to the specific nominal vehicle. The user may choose to use scaling or to leave the component mass as originally input. A graph comparing the part mass to mass for other benchmark vehicles is also provided in this step.

Step 3- The nominal vehicle is resized by substituting the competitor component for the original. This substitution will require other vehicle systems to be resized in response to the mass difference in the original and competitor components. Secondary mass change is the primary tool used in this step. The user may choose the method for secondary mass change, and which subsystems are free to be resized.

At this point, two vehicles have been defined allowing a comparison at the vehicle system level.

Step 4- Several metrics are calculated and compared for the two vehicles. These are:

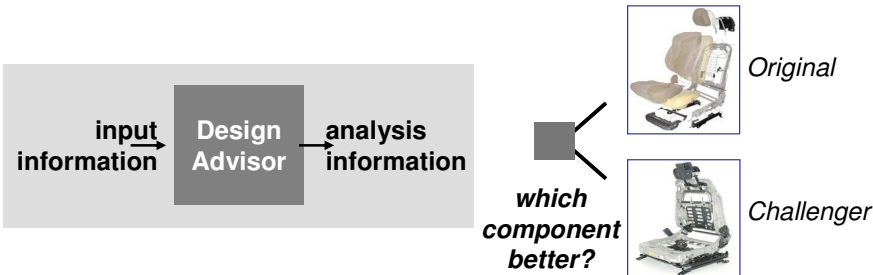
1. Mass change (primary and subsystem resizing)
2. Cost change (primary and subsystem resizing)
3. Changes in fuel use and greenhouse gas
 - Material production greenhouse gas
 - Use Phase greenhouse gas
 - Recycling greenhouse gas credit
 - Life cycle total greenhouse gas
 - Fuel consumption
 - Life time fuel use
 - Life time fuel cost

Because much of the information used in these calculations is approximate, a final step is provided:

Step 5- A sensitivity analysis of how the metrics change in response to small changes in several parameters.



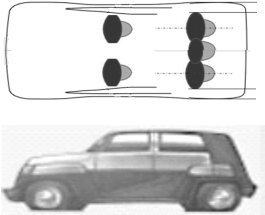
2- Quick Start Application Example

As a sample application of the *Design Advisor*, consider a decision to use either a Steel driver’s seat frame or a lighter mass magnesium seat frame. As is often the case in vehicle design, the decision must be made before complete information is available for the vehicle or the seat frames.



Context for use of Design Advisor

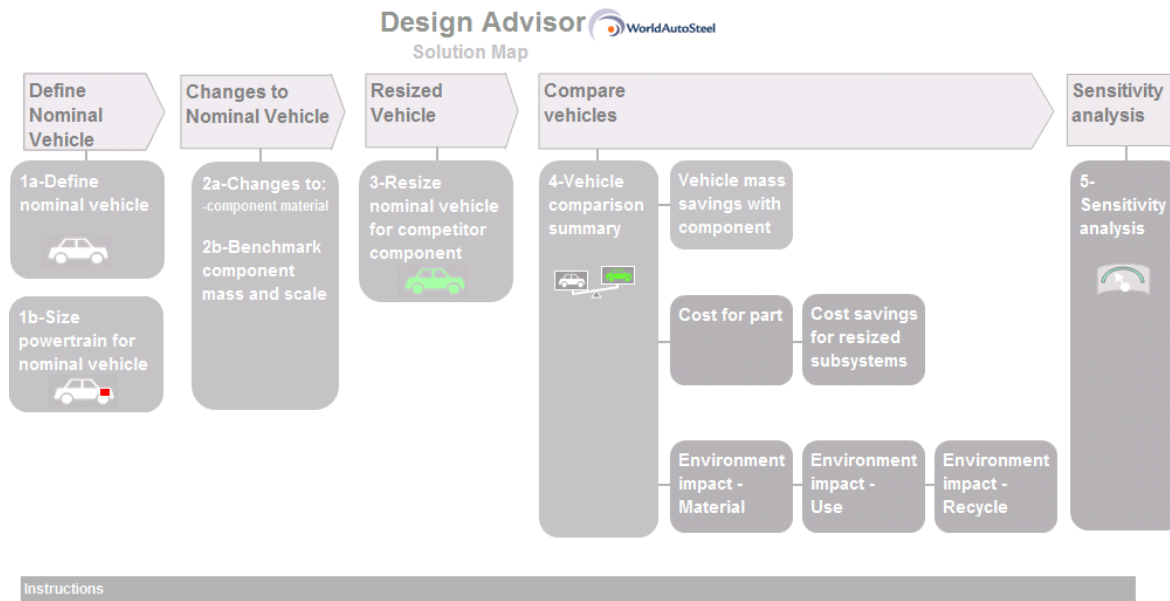
The available input information for this case study is shown below.

Component: Seat Frame		Vehicle Parameters
		
Original Component	Competitor Component	
Steel Stamped 17 kg total seat mass 10 kg frame mass	Magnesium, High pressure die cast 13 kg total seat mass 6 kg frame mass	Sedan/Hatchback 5 passenger 100 kg cargo OAL=4.7 m OAW=1.8 m New architecture Internal Combustion-gasoline Powertrain is fixed and will not change 6.8 liter/100 km (HYZEM schedule) Life time range =155,000 km

Input information for example application

In subsequent sections, the *Design Advisor* will be used to estimate the mass, cost, and greenhouse gas impacts on the vehicle system.

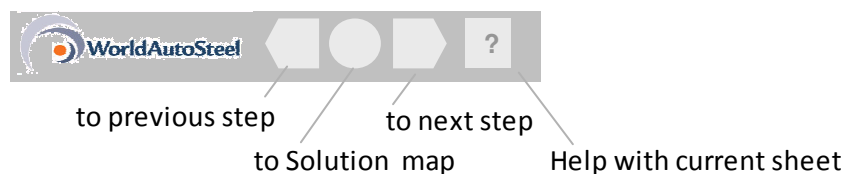
Solution Map for navigating through the Design Advisor- The first sheet of the *Design Advisor* is the *Solution Map*. This map shows the sequence of solution steps to be followed to arrive at the final results. The analysis is ordered by moving from left to right through all steps in numerical order.



Sheet: Solution Map

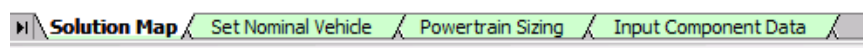
The user can use the *Solution Map* sheet to move through building process from left to right by clicking on the icons, inputting data, then using the 'Back to Solution Map' button found on each sheet.

An alternative method for navigation is to use the buttons found on each sheet in the upper right corner.



Navigation buttons

A final alternative is to use the sheet tabs at the bottom of the screen moving from left to right.



Sheet tabs

Conventions have been adapted to display information:

- Fields in **light blue** indicate information to be input by the user. In some cases, drop-down lists, check boxes, and slider bars are also provided for data input.
- Fields marked in **orange** indicate values calculated in that sheet or in a prior sheet. Pre-loaded parameter values are also shown in orange.
- On any sheet, by scrolling down, the pre-loaded parameter values may be found, there are also listed in the Appendix. With normal use, these parameters are not changed and there is no need to view this information.

These instructions are summarized on the *Instructions* sheet accessed from the *Solution Map*, bottom bar. Note also at the bottom of the *Instructions* sheet, the cell protection may be turned off. This allows selecting and changing any cell in the workbook. Under normal use, the protection should be *On* to prevent accidentally overwriting a formula.

Instructions

The purpose of the *Design Advisor* is to assess the impact on the overall vehicle system of a change to a component. Several metrics are calculated in the areas of mass reduction, change in cost, and environmental impact.

The user is stepped through the process of building two vehicles; a nominal vehicle with the original component, and a resized vehicle with the competitor component. The performance of these two vehicles is then compared.

The user can use the *Solution Map* sheet to move through building process from left to right by clicking on the numbered icons, inputting data, then using the *To Solution Map* button found on each sheet. An alternative method is to use the navigation icons at the top of each screen.

The *Results and Sensitivity* sheet displays a comparison of the nominal and resized vehicles using several metrics (mass, cost, CO2). A sensitivity study may be run by varying several key parameters.

The intent of the *Design Advisor* is to provide early guidance in whether to pursue the component technology. The metrics are necessarily approximate and use First Order Analysis, FOA, to make the estimates. If a decision is made to proceed with the technology, follow-up calculations with more precise analysis tools should be used.

Conventions have been adapted to display information:

- Fields marked in light blue indicate information input by the user
- Numbers in orange indicate values calculated in a prior step and carried over for reference.

Optional information: The variables and the sheet on which they are introduced are listed under the tab *Variable Map*.

Protection ON

On Off

Color coding of cells and numbers

Spreadsheets are protected to avoid accidental changing of cells. Normally leave Protection ON

Sheet: *Instructions*

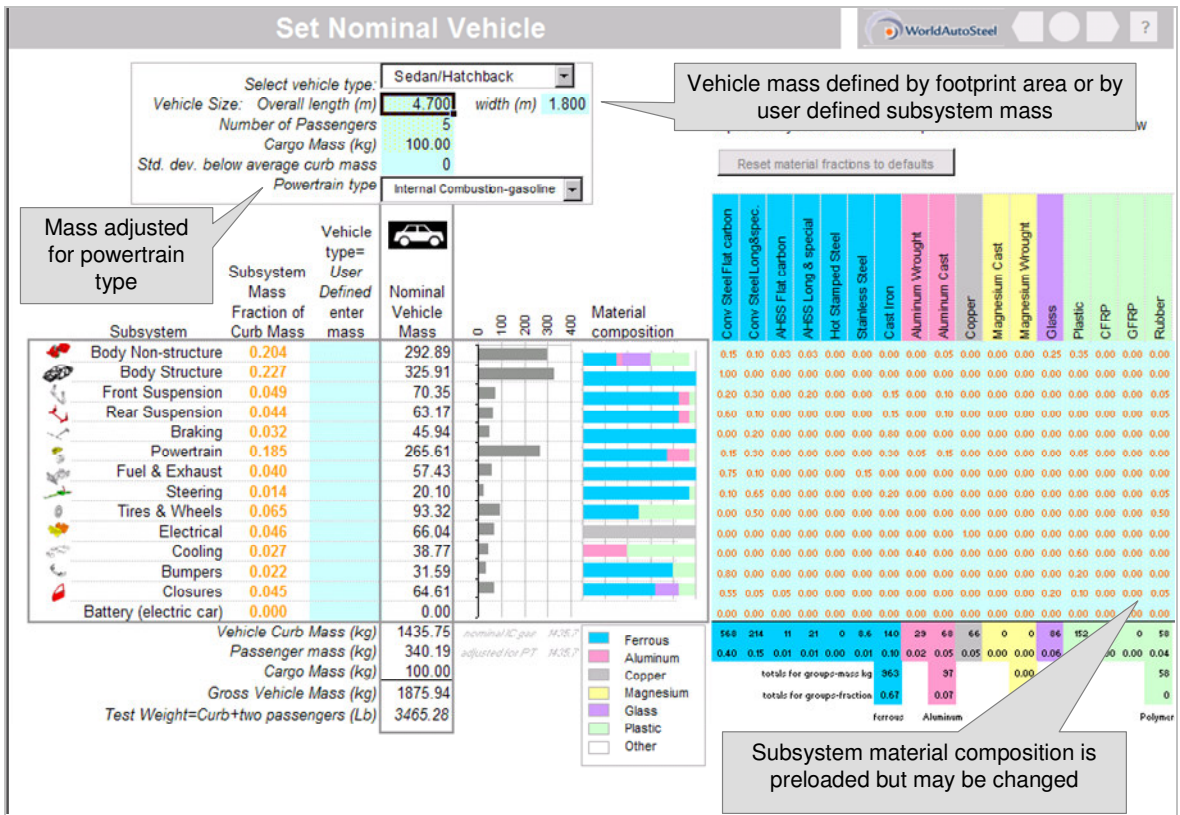
We will now step through the Seat Frame case study. Refer to the illustration at the beginning of Section 2 for the input information.

Step 1a: Create nominal vehicle- The user now defines the nominal vehicle on which to ‘install’ the original component. Selecting the left icon on the *Solution Map*, ‘Define nominal vehicle’, the user is taken to the sheet shown below.

Here the user identifies the vehicle type and size using length and width. The number of passengers and cargo mass are also input. A powertrain type is selected (*internal combustion-gasoline, internal combustion-diesel, parallel hybrid, fuel cell, plug-in electric, or battery electric*). Based on these inputs, the mass for vehicle curb condition, for GVM, and for each subsystem are estimated. These estimates are for a nominal vehicle. If the user desires a lighter-than-average vehicle, the number of standard deviations below the nominal value may be entered.

To the right of this sheet is a large matrix—the vehicle Bill of Materials (BOM). This matrix indicates the material content for each subsystem. The default BOM represents a typical contemporary vehicle. This matrix may be altered by the user.

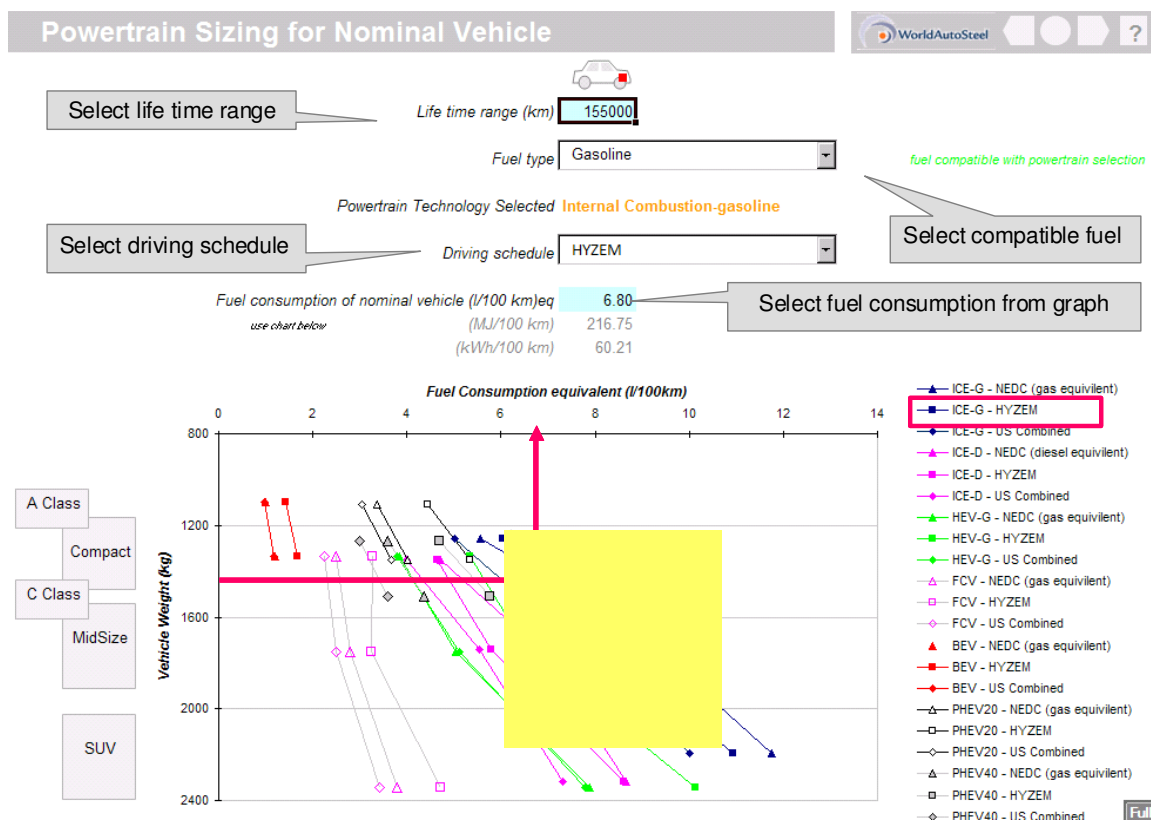
In the upper right corner of each sheet is a link back to the *Solution Map* (circle), a right facing arrow for the next step, a left facing arrow to go back to the previous step, or a question mark for help with this sheet.



Sheet: Set Nominal Vehicle

Step 1b: Size powertrain for nominal vehicle- As the final step in setting the nominal vehicle, the user sizes the powertrain. On this sheet the user enters life-time range, the fuel type consistent with the selected powertrain (*gasoline, diesel, E85, hydrogen, biodiesel, electricity*), the driving schedule (*NEDC, HYZEM, US Combined*), and the fuel consumption.

Results of simulations for the vehicle types, powertrain combinations and driving schedules have been loaded as parameters [5, 6, 7]. A chart of fuel consumption vs. vehicle mass is provided to select the appropriate fuel consumption consistent with this simulation data. Note that in these simulations vehicle mass is associated with a specific vehicle type (A & C class, Compact, Midsize, SUV). Front area, drag coefficient, and gradability are consistent with the vehicle type. For this example, note how the calculated vehicle mass (yellow dot on graph below) falls on the curve for Internal Combustion-gasoline, HYZEM schedule.



Sheet: Powertrain Sizing

Step 2a: Input component data for original and competitor component- The primary input data for the *Design Advisor* is a description of the original and competitor components. This required data includes component mass, mass of the part of interest within the component, the value of any mass drivers for this component, part material and primary shaping process. This set of data is required for both the original and the competitor design concepts.

In the screen print below, the user has navigated using the *Solution Map* by clicking the second from left icon 'Changes to Component'. All inputs are either list boxes, or indicated with a light blue field. This convention is used throughout the *Design Advisor*.

Metric units are used exclusively throughout the Design Advisor. The 'Front Seat Frame' has been selected from a list of 16 components for which benchmark data exists. Once the component name has been identified, the corresponding subsystem is shown to the right. Mass for the total component and for the part within the component is entered (the part may be a weldment or assembly of the same material).

Finally, the part material and the primary shaping process are selected from lists. These will be used for cost estimation and in the material and recycling estimates of greenhouse gas. Note the message on material/process compatibility. If a warning message is displayed, the results will not be valid.

Changes to a selected component

Units: Metric m, km, kg, (liter/100km), MJ, kWh

Component Name Front Seat Frame Component subsystem: Body Non-structure

Mass Driver for component
No mass driver

Component data
enter data for a single component

	original component	competitor component
mass of total component (kg)	17	13
mass of part within component (kg)	10	6
part material	Steel-Conventional	Magnesium Cast
part primary shaping process	Steel Stamping	NonFerrous Die Casting

☐ Folded ☒ Shallow ☐ Deep Draw

process compatible

Mass driver for Non cycle 0 Enter same as above if unknown

scaled mass 17.00 13.00

mass 10.00 6.00

Front Seat Frame mass (kg)

No mass driver

Complexity for stampings

Steel-Conventional

Steel-AHSS

Steel-Hot Stamped

Steel-Stainless

Cast Iron

Aluminum Wrought

Aluminum Cast

Steel Stamping

Steel TWB Stamping

Steel Hot Stamping

Steel open roll form

Steel Tube Hydroform

Steel Forging

Iron Casting

Full

Sheet: Input Component Data

Step 2b: Scale component for nominal vehicle- In the same input sheet, benchmark data is shown on the right side which allows comparison of the input mass data with data from several other vehicles.

Also, on this sheet, the component may be scaled based on mass drivers relevant to this component (for the case of the seat frame, there are no mass drivers). To illustrate the use of mass drivers and component scaling, below is an illustration for a hood. Here the mass driver is hood area. If the hood area on the nominal vehicle (1.5 m^2 in this example) is different than that used in the input data (2 m^2 in this example), the hood mass is scaled based on the mass driver. The scaled mass for components and parts shown at the bottom of the sheet will be used in subsequent calculations.

If the mass driver values are unknown, or if scaling is not desired, the user by enter the same arbitrary value for both and no scaling will be applied (for example *Hood Area used to size component*=2, and *Mass driver for Nominal Vehicle*=2).

Note also that the part and component data are always entered for one unit. The Design Advisor will adjust the mass for the number of units per vehicle. For example, referring to the above illustration for the seat frame. The seat frame data is entered for one seat. The software will account for the fact that a vehicle will have two front seats as seen at the bottom of the sheet.

Changes to a selected component

Units: Metric
m, km, kg, (liter/100km), MJ, kWh

Component Name

Hood Frame

Component subsystem:

Closures

Mass Driver for component

Hood Area used to size component

2 m²

Component Data

enter data for a single component

★ original component

17

★ competitor component

12

15

10

part material

Steel-Conventional

Magnesium Cast

part primary shaping process

Steel Stamping

NonFerrous Die Casting

☐ Folded
 ☒ Shallow
 ☐ Deep Draw

process compatible

Scaling mass data

Mass driver for Nominal Vehicle

1.5 m²

scaling exponent

1.240

scaled component mass

11.90

scaled part mass

10.50

Enter same as above if unknown

8.40

7.00

Units per vehicle

1

Scaled mass of component set

11.90

Scaled mass of part set

10.50

Scaled mass of component set

8.40

Scaled mass of part set

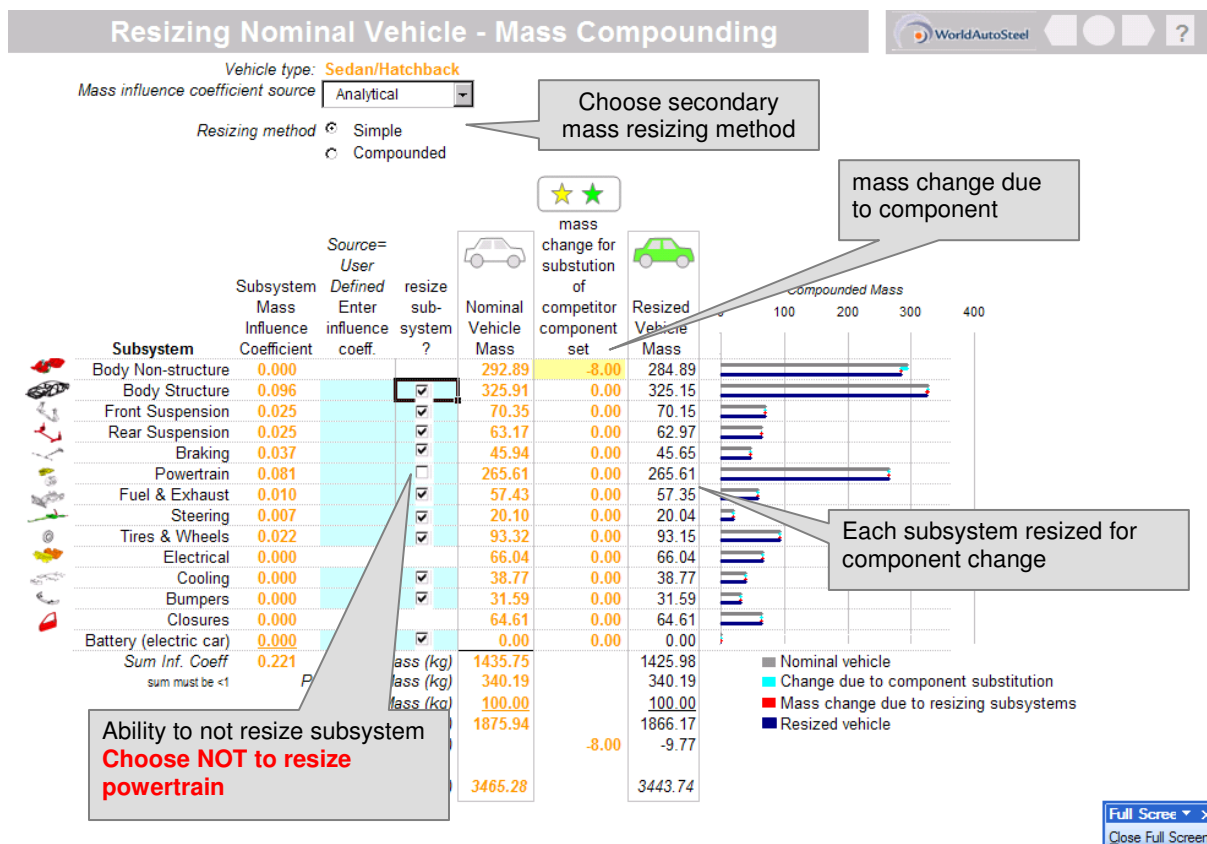
7.00

Sheet: Input Component Data
Example: Hood having Mass Driver of Area

Step 3: Define resized vehicle by resizing nominal vehicle- The previous steps have defined a nominal vehicle having the original component. In this sheet, that vehicle is resized for the competitor component. This includes adjusting the mass of some subsystems which are mass dependent. The primary tool used here is secondary mass analysis.

Little input is required of the user. The software inserts the primary mass change (the difference in the adjusted original component and competitor component masses) at the appropriate subsystem. The user enters the source for the secondary mass coefficients (*Analytical, Regression, Ratio, or User Defined*), and the resizing method (*Simple, Compounded*). The user can further specify which subsystems to consider in the resizing. For this example, the all subsystems can be resized with the exception of the powertrain.

Using mass influence coefficients the vehicle is resized. This resized vehicle will be compared with the nominal vehicle in subsequent steps.



Sheet: Mass Compounding

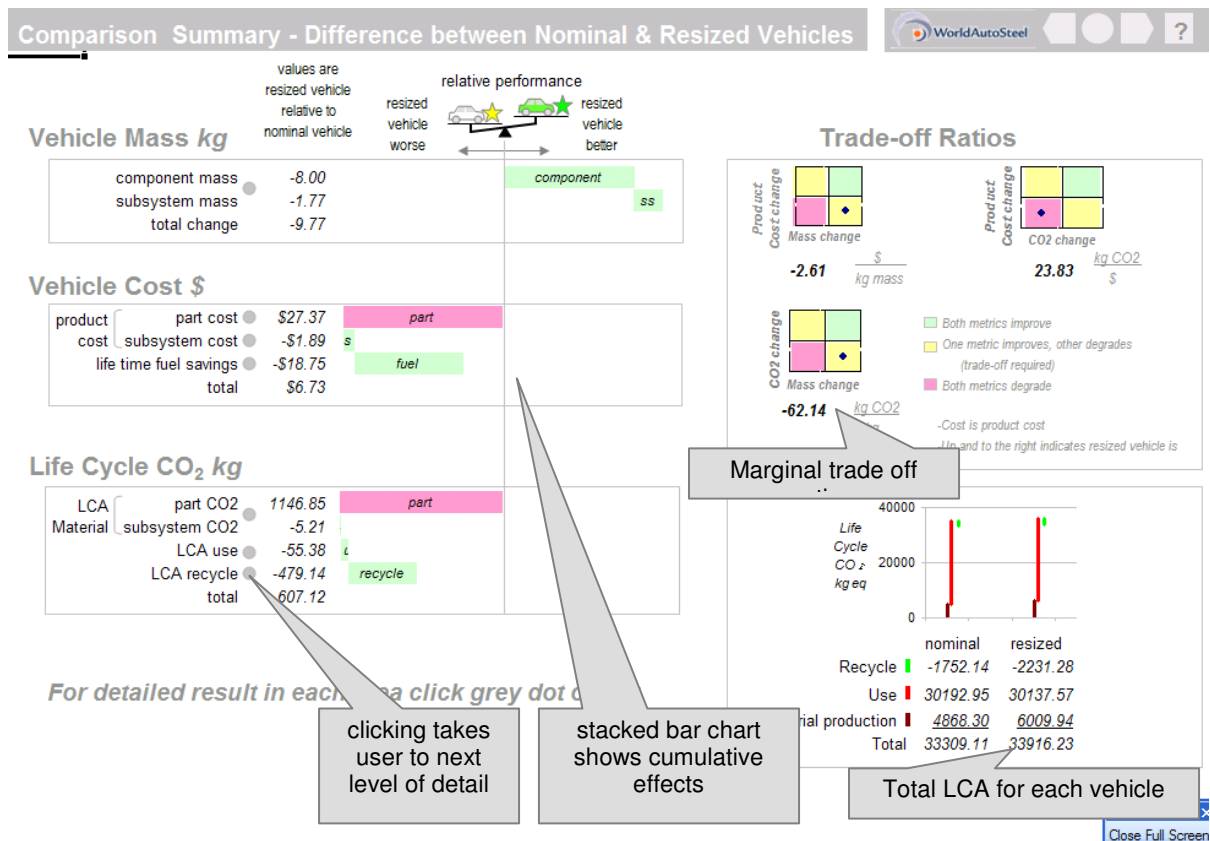
Step 4: Comparison summary – The Comparison Summary shows is a high-level summary of the results for mass, cost, and greenhouse gas. Each value shown on the left is the difference between the Resized vehicle and the Nominal vehicle. Negative values indicate the Resized vehicle is preferred to the Original vehicle.

Bar charts are provided in each area for a quick assessment of performance. The bars are additive as vectors, see illustration on next page. If the sequence of bars terminates on the right side, the resized vehicle is preferred; on the left side, the nominal vehicle is preferred. Green bars indicate that metric is favorable for the resized vehicle, red for the nominal vehicle.

Often the individual metrics are in conflict: one improves while another degrades. To capture this behavior, trade-off ratios are provided. See the illustration at the bottom of the next page for a definition of trade-off ratios.

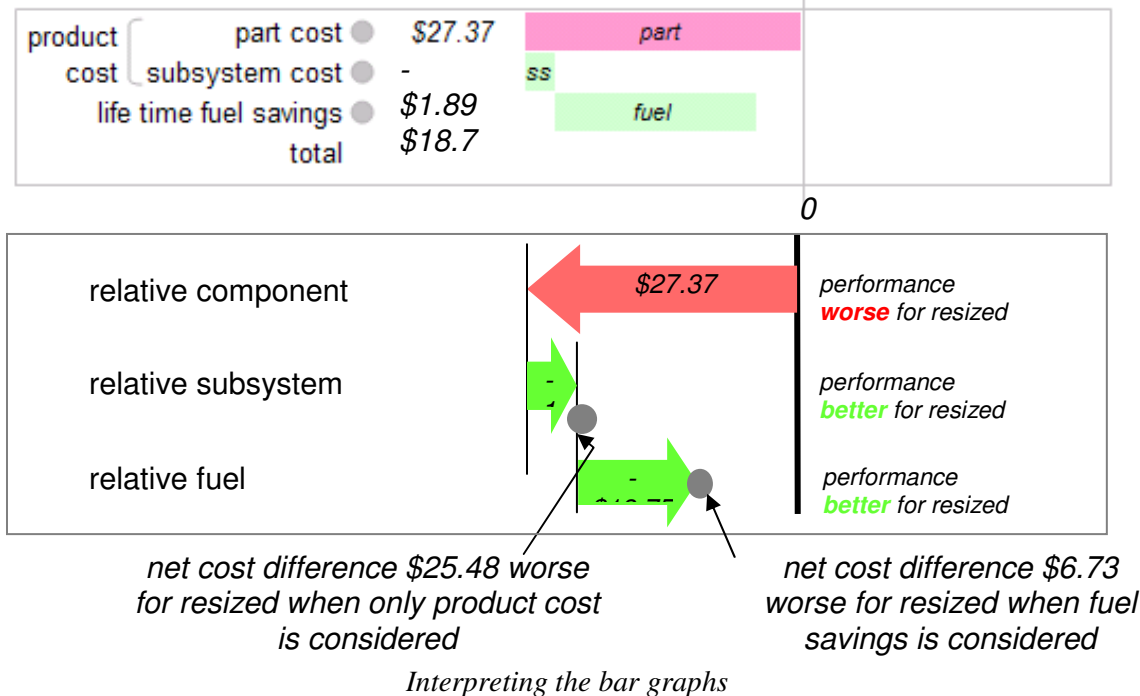
Finally in the lower right corner, life cycle greenhouse gas estimates are provided for each vehicle. We are primarily interested in the differences however these absolute values are useful for comparison with other sources.

This sheet is a summary. By clicking either on a specific bar, or by clicking on the gray dot next to the metric name, a sheet with detailed results for that area will be brought up.

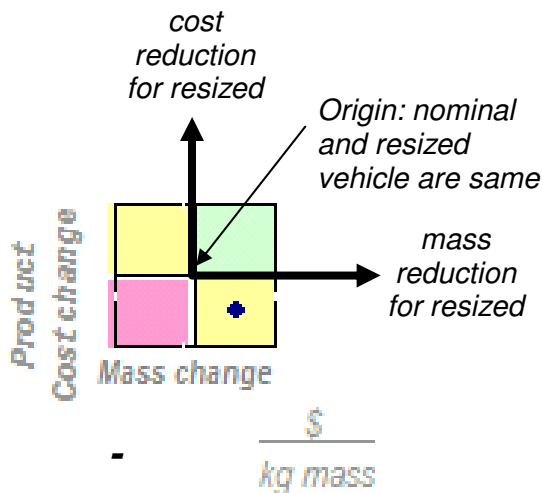


Sheet: Comparison Summary

Vehicle Cost \$



Trade-off



$$T.O.R. = \frac{\Delta \text{product cost}}{\Delta \text{mass}}$$

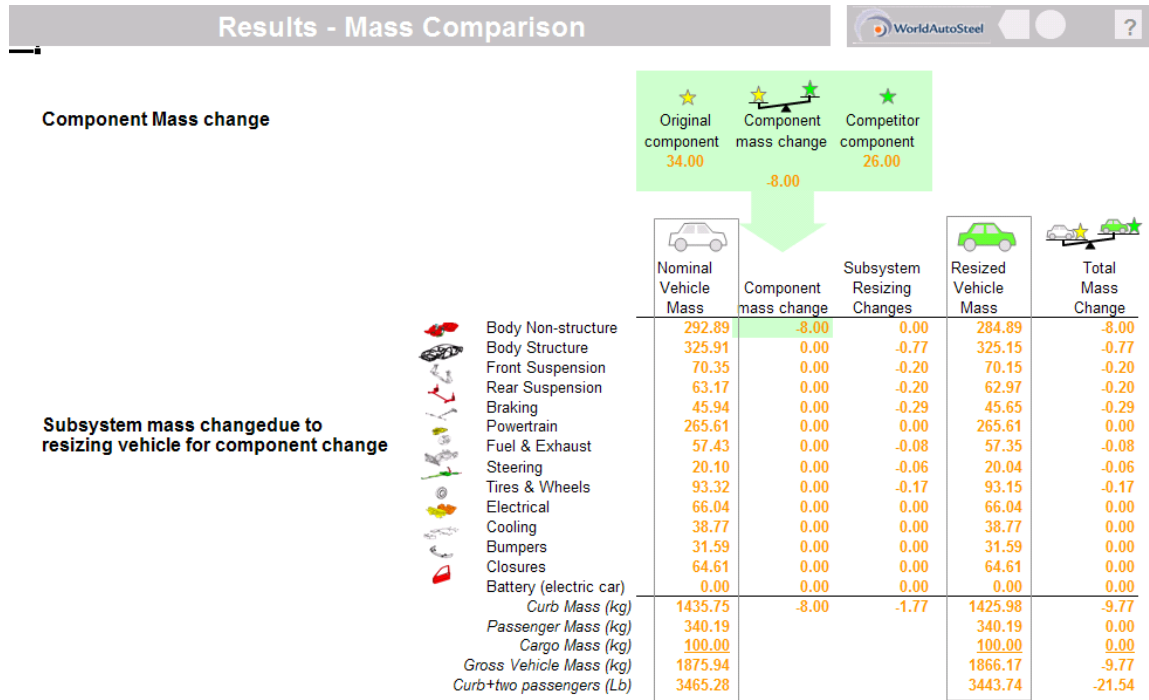
+\$27.37-\$1.89=\$25.48 increase in cost for a 9.77 kg mass reduction

$$T. O. R. = \frac{\$25.48}{-9.77 \text{ kg}} = -2.61 \frac{\$ \text{ spent}}{\text{kg reduced}}$$

- quadrant where both metrics are better for resized vehicle relative to nominal
 - quadrant where both metrics are worse for resized vehicle
 - quadrant where one metric is better, one worse for resized vehicle
- Trade-off ratio significant**

Definition of Trade-off ratios

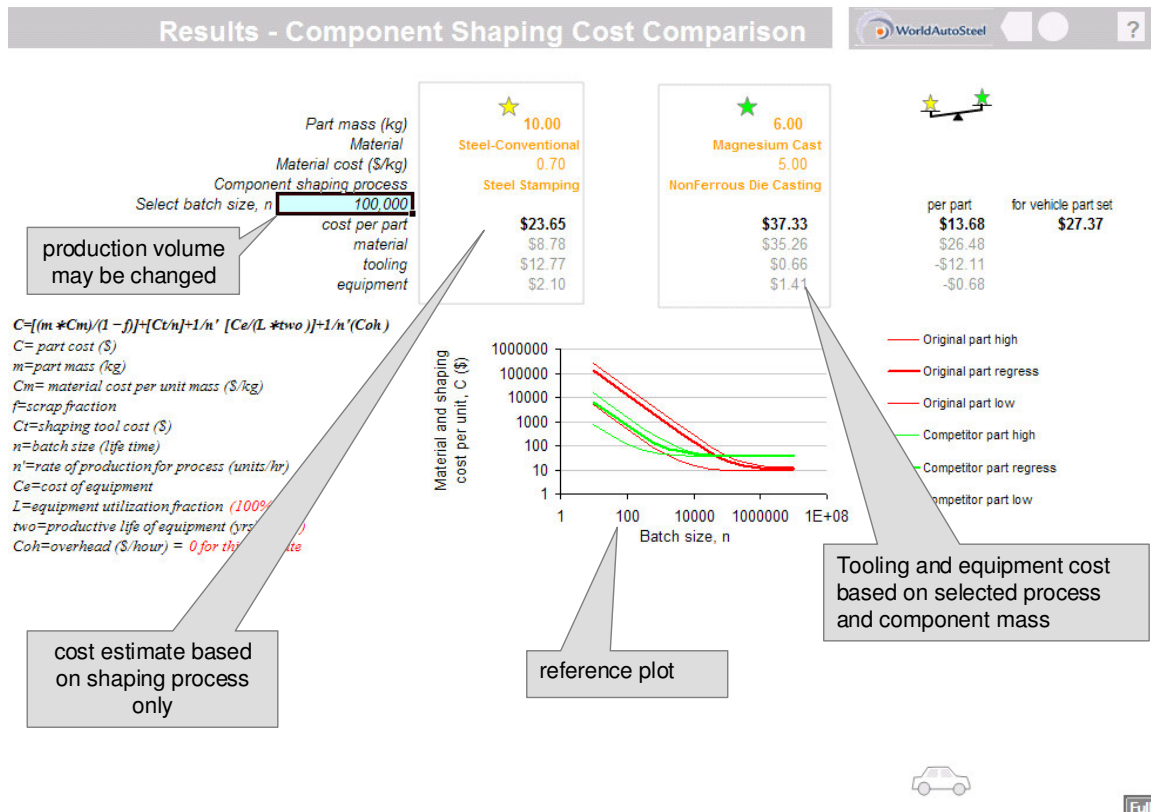
Detailed Results: Mass comparison- In this detailed results sheet, mass is compared for both primary changes (considering only component), as well as subsystem resizing changes between the nominal vehicle and resized vehicle. This sheet requires no inputs.



Sheet: Mass Change

Detailed Results: Part shaping cost comparison- Cost is estimated for the original and competitor parts and includes material, tooling, and equipment cost for the primary shaping process only. All costs are based on the part mass, material, and shaping process. Therefore this is an approximate cost for comparison purposes only.

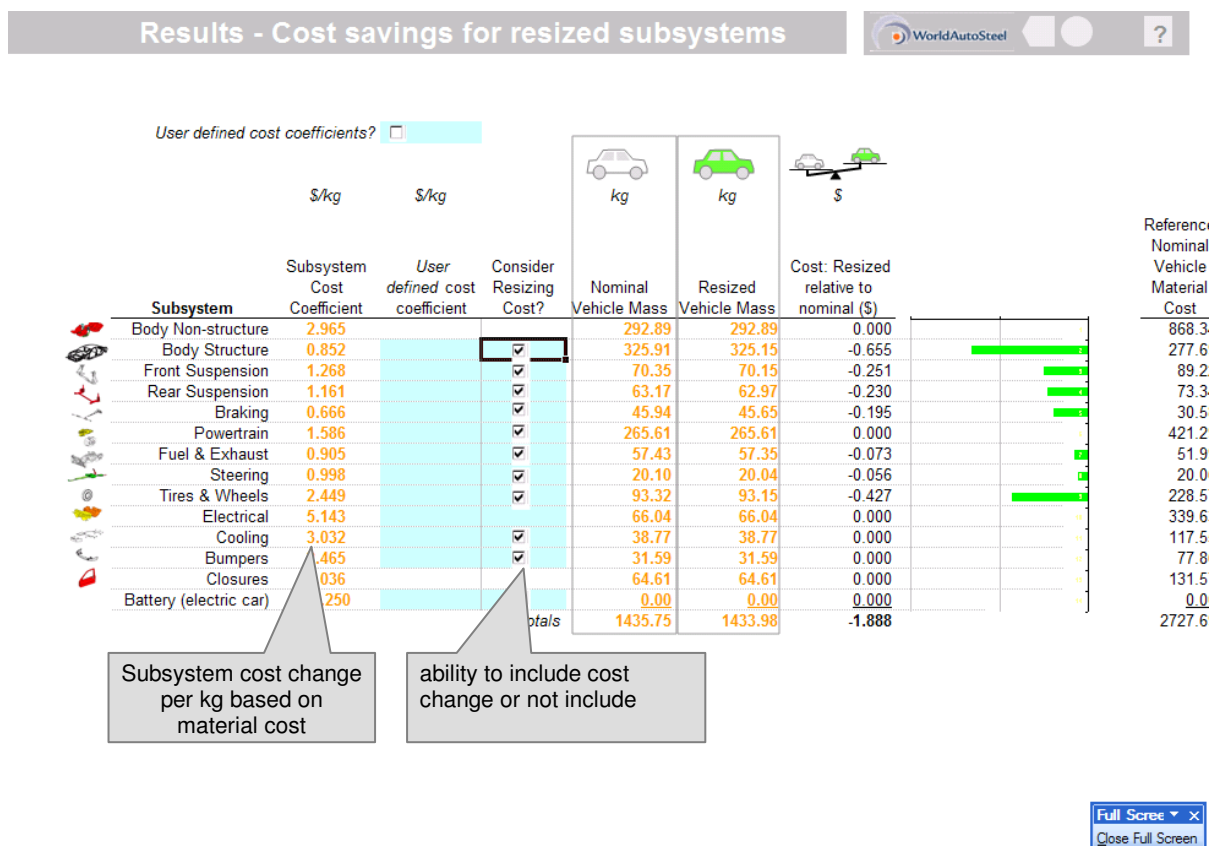
A graph showing part cost dependency on manufacturing batch size is included for both the original and competitor part. Often these will cross-over, and the user may enter a batch size other than the default 100,000 units.



Sheet: Primary Cost

Detailed Results: Cost savings for resized subsystems - Due to the primary change in component mass, the resized vehicle will have subsystem mass changes. These changes in mass will incur subsystem resizing cost changes. The resizing cost of changing a subsystem is estimated as a factor—(\$/ unit mass change). This factor will be different for each subsystem and is based only on material cost changes.

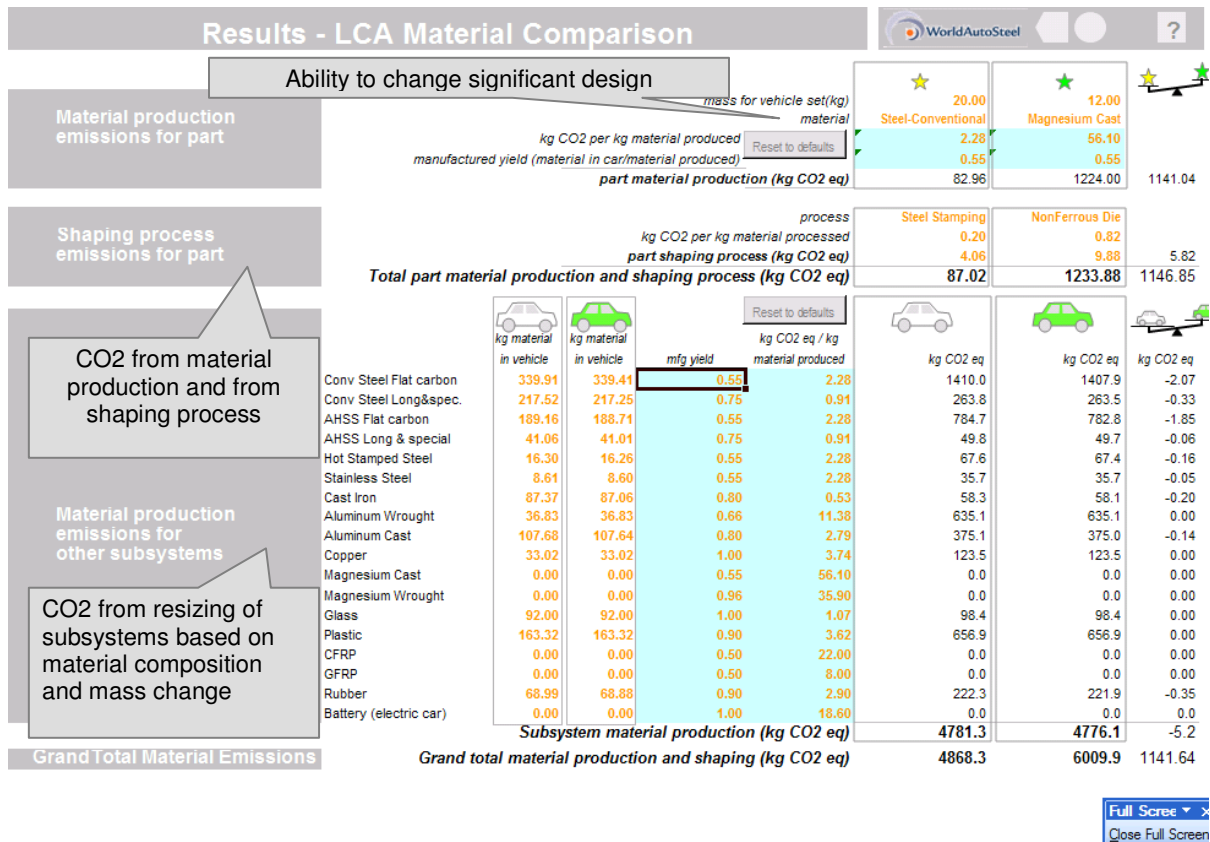
The user may define cost coefficients, and also decided which subsystem to consider resizing costs.



Sheet: Subsystem resizing Cost

Detailed Results: LCA Material comparison- Greenhouse gas—CO₂—in the production of the vehicle material is calculated. The part CO₂ is estimated based on the materials in the original and competitor components. CO₂ for the primary shaping process is also estimated. A subsystem resizing CO₂ value is based on the material content for each subsystem. The grand total CO₂ for material production is the sum of the part, shaping process, and subsystem resizing values. For this example, CO₂ has been increased for the resized vehicle.



Key parameters of CO₂/unit of material mass and manufacturing yield may be changed by the user.



Sheet: LCA-Material

Detailed Results: LCA Use comparison- The greenhouse gas generated during the use phase are estimated, as well as energy use. The user may keep powertrain size fixed between the nominal and resized vehicle, or may resize the powertrain to achieve the same acceleration performance between the two vehicles. In both cases, the fuel consumption changes are based on a fuel consumption mass reduction value which is determined by simulation [5, 6, 7].





Results - LCA Use Comparison

ability to resize
powertrain for
constant
performance

Selected fuel **Gasoline**
 Selected powertrain technology **Internal Combustion-gasoline**
 Selected driving schedule **HYZEM**
 Selected fuel consumption **6.80 l/100km eq** **216.75 MJ/100km**
 Selected life time range **155000 km**
 Liquid fuel reduction value **0.1277 l/100km eq/100kg** **4.0693 MJ/100km/100kg**
 Electricity consumption reduction value **0.0000 l/100km eq/100kg** **0.0000 MJ/100km/100kg**
 Vehicle mass difference **-9.7696 kg**
 Resize powertrain for equal performance? ☒ **FALSE**

Fuel consumption
Reduction Value based on
fka models

Fuel Consumption	Liquid fuel 	Electricity	Liquid fuel 	Electricity	Liquid fuel 	Electric 
Fuel Consumption	6.800 l/100km eq	0.000 kWh/100km	6.788 l/100km eq	0.000 kWh/100km		
	216.750 MJ/100km	0.000 MJ/100km	216.352 MJ/100km	0.000 MJ/100km		
Life time fuel use by source	10540 liter	0 kWh	10521 liter	0 kWh	-19.33	0.
	335963 MJ	0 MJ/90%charge eff	335346 MJ	0 MJ/90%charge eff		
Total vehicle fuel demand-all sources	335,963 MJ		335,346 MJ		-616.21	
Fuel Consumption						
Unit fuel cost	0.97 \$/l	0.97 \$/kwhr	0.97 \$/l	0.97 \$/kwhr		
Life time fuel cost	\$10,224 \$	\$0 \$	\$10,205 \$	\$0 \$	-18.75	
Total Life time cost	\$10,224 \$		\$10,205 \$		-14.48	
Discount rate %/yr	5.0%					
Present value fuel cost (10yr)	\$7,895 \$		\$7,880 \$			
Tank to Wheel CO2 eq						
Tank to wheels CO2 per unit fuel	0.072 kg CO2eq/MJ		0.072 kg CO2eq/MJ			
Life time CO2 from liquid fuel use	24156 kg CO2eq		24111 kg CO2eq		-44.31	0.
Well to Tank CO2 eq						
Fuel production energy per unit output	0.210 MJ/MJ	0.210 MJ/MJ	0.210 MJ/MJ	0.210 MJ/MJ		
CO2 per unit energy production	0.018 kg CO2eq/MJ	0.018 kg CO2eq/MJ	0.018 kg CO2eq/MJ	0.018 kg CO2eq/MJ		
Fuel production energy	70552 MJ	0 MJ	70423 MJ	0 MJ		
CO2 from fuel production by type	6037 kg CO2eq	0 kg CO2eq	6026 kg CO2eq	0 kg CO2eq		
Life time CO2 from fuel production	6037 kg CO2eq		6026 kg CO2eq		-11.07	
Well to Wheel Grand total						
	30,193 kg CO2eq		30,138 kg CO2eq		-55.38	
	406,515 MJ		405,769 MJ			

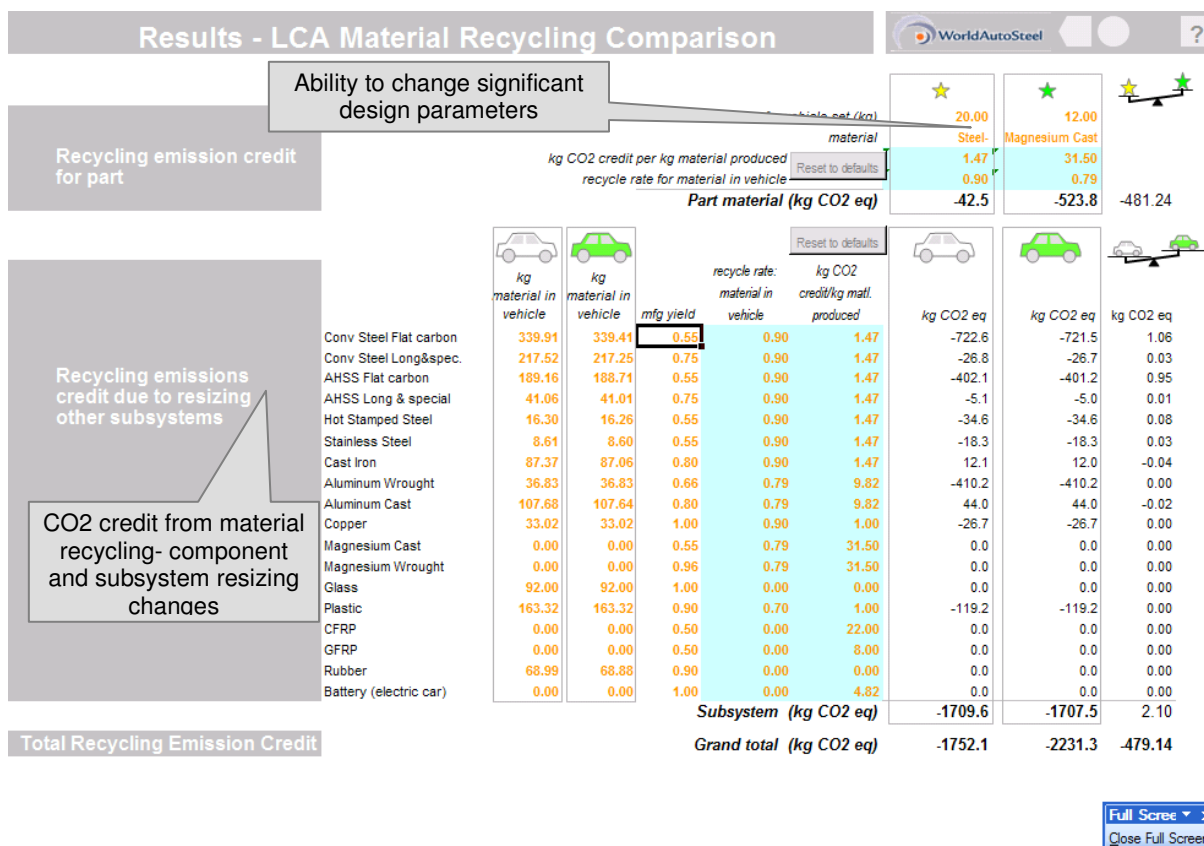
Full Screen

Close Full Screen

Sheet: LCA-Use

Detailed Results: LCA Material Recycling comparison- Greenhouse gas credit due to recycling of the vehicle material is calculated. As in the material production calculation, the primary CO₂ is estimated based on the materials in the original and competitor components. A subsystem resizing CO₂ value is based on the material content for each subsystem (the same content is used as in the material production CO₂ estimate). The total CO₂ credit for material recycling is the sum of the part and subsystem resizing values.

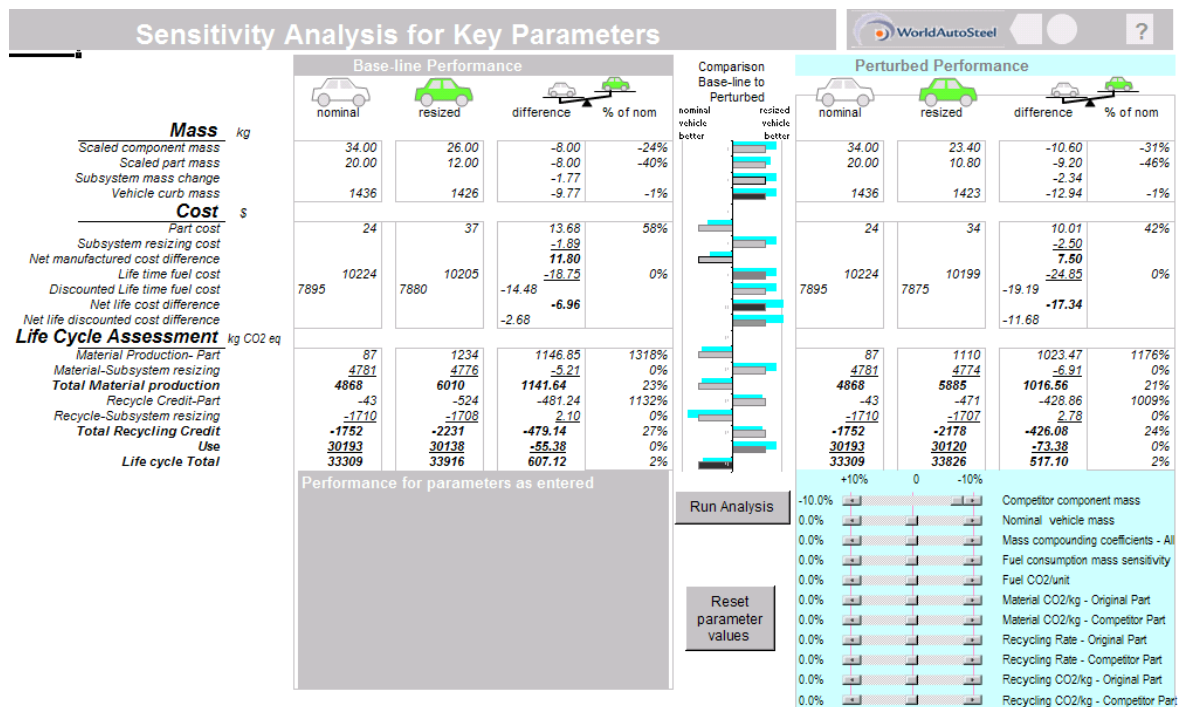
Key parameters of CO₂ credit/unit of material mass and recycle rate may be changed by the user.



Sheet: LCA-Recycle

Step 5: Sensitivity Analysis- The Sensitivity Analysis sheet provides a summary of all estimates (Base line performance on left side of sheet for input values). It also allows the user to see how small variations in select parameters affect performance (Perturbed Performance on the right side of the sheet). In the graph, gray bars indicate directionally the base-line analysis values while the blue bars indicate the perturbed values.

To perform a sensitivity analysis, first click the *Reset parameter values*, then click *Run Analysis*. This will make Perturbed Performance the same as the base. Now change key parameters using the sliders, then click *Run Analysis*. The Perturbed Performance will now reflect the changes made. This analysis is particularly useful in seeing if a result will 'flip' in preference—the blue bar will be on the opposite side of the center line. This indicates that the preference for the components is not strong and that further detailed analysis is needed.



Sheet: Sensitivity Analysis

The table below is a summary of the specific information input on each sheet of the *Design Advisor*. Bold font indicates required inputs. Red indicates important parameters which can be changed from Results Summary sheet.

Excel Sheet

Information input on sheet

1a. Set Nominal Vehicle

- **vehicle type**
- **length and width**
- **number of passengers**
- **cargo mass**
- (optional) standard deviation from average curb mass
- **powertrain type**
- (optional) subsystem masses

1b. Powertrain Sizing

- **life time range**
- **fuel type**
- **driving schedule**
- **nominal vehicle fuel consumption**

2a. Input Component Data

2b. Size Component for nominal vehicle

- **component name**
- **mass driver value used to size component**
- **component and part mass**
- **component material**
- **shaping process**
- **mass driver for nominal vehicle**

3. Resizing Nominal Vehicle

(sheet Mass Compounding)

- **influence coefficient source**
- **resizing method**
- **resize specific subsystems (yes/no)**
- (optional) subsystem influence coefficients

Results-Component Shaping Cost

(sheet Component Cost)

- **batch size**

Results-Cost savings for resized subsystem

(sheet Subsystem Cost)

- (optional) consider cost for specific subsystems (yes/no)
- (optional) subsystem cost coefficients

Results-LCA Material Comparison

(sheet LCA-Material)

- (optional) manufacturing yield
- (optional) GHG/unit material coefficient

Results-LCA Use Comparison

(sheet LCA-Use)

- **Resize powertrain for equal performance (yes/no)**
- (optional) Discount rate for fuel cost

Results-LCA Recycling Comparison

(sheet LCA-Recycle)

- (optional) manufacturing yield
- (optional) GHG/unit recycle coefficient

3- Technical Description

In this section, the models used to in the *Design Advisor* are described. These first order analysis models were selected to provide enough accuracy to support the A vs. B selection decision, and also because they require only that input information which would be available during the early design stages.

3.1 Mass Estimation for the Nominal Vehicle- Often the curb mass for the vehicle is unknown and must be estimated. The plan view area of the vehicle (Length x Width) can be used to make this estimation,

$$(Curb\ mass) = \beta_1 (plan\ view\ area) + \beta_0$$

where

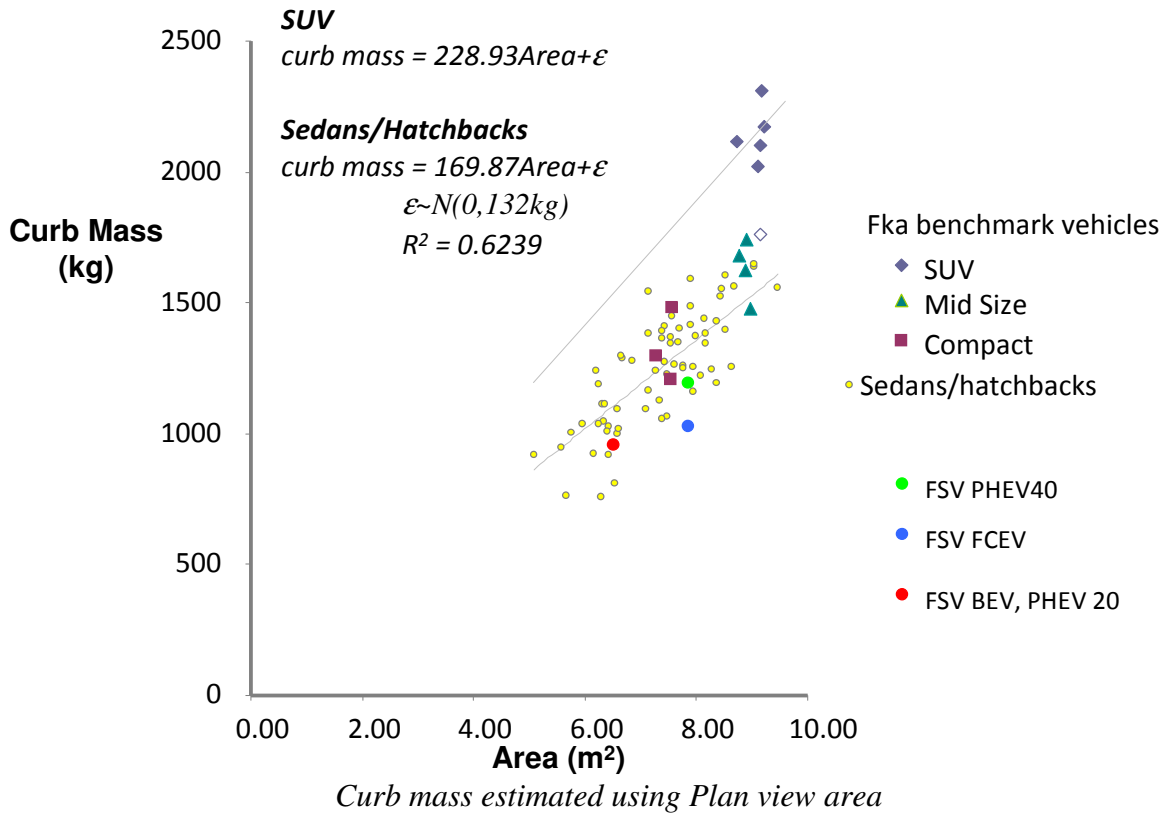
m'_{CURB} = estimated curb mass (kg) for base gasoline IC, sedan/hatchback, FWD, BFI

A_{PLAN} = Plan view area of vehicle (length x width) (m^2)

β_0, β_1 = coefficients estimated by regression

ϵ = residual error $N(0, \sigma)$

Data from several sources were used to fit the above expression, see below [1, 4, 5, 11, 12].



With curb mass determined, the mass for each subsystem may be taken as a fraction of the estimated curb mass.

$$\bar{\phi} = \begin{bmatrix} \phi_1 \\ \phi_2 \\ \vdots \\ \phi_n \end{bmatrix}, \quad m'_{CURB} \bar{\phi} = \begin{bmatrix} m_1 \\ m_2 \\ \vdots \\ m_n \end{bmatrix}$$

where

ϕ_i = mass fraction relative to curb mass for subsystem i

for the reference vehicle (IC gasoline), $\sum \phi_i = 1$

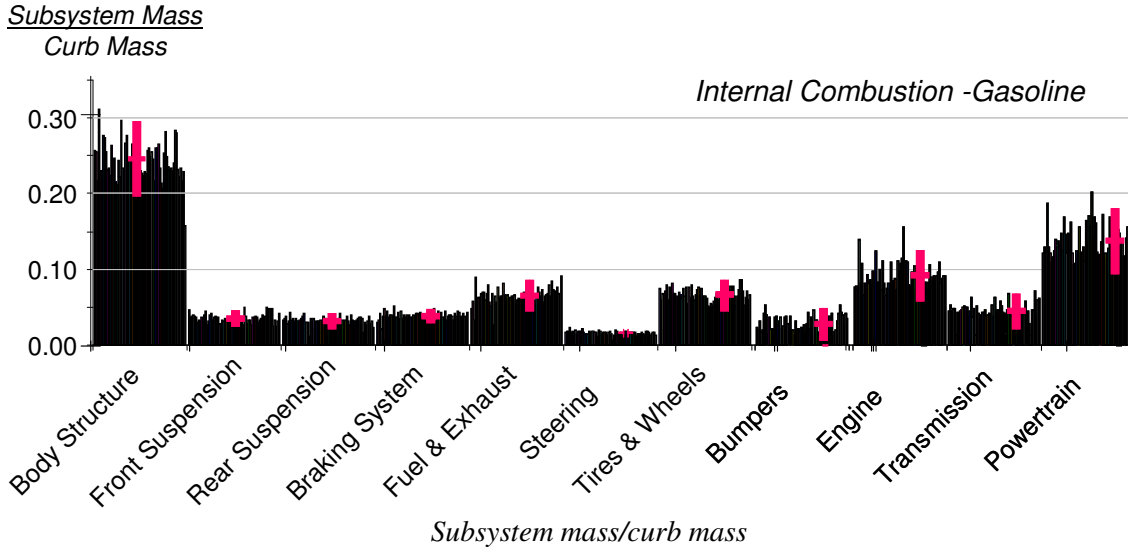
for other powertrain types, $\sum \phi_i$ may be smaller or larger than one

m'_{CURB} = curb mass (kg) of reference IC-gasoline vehicle estimated by plan view area

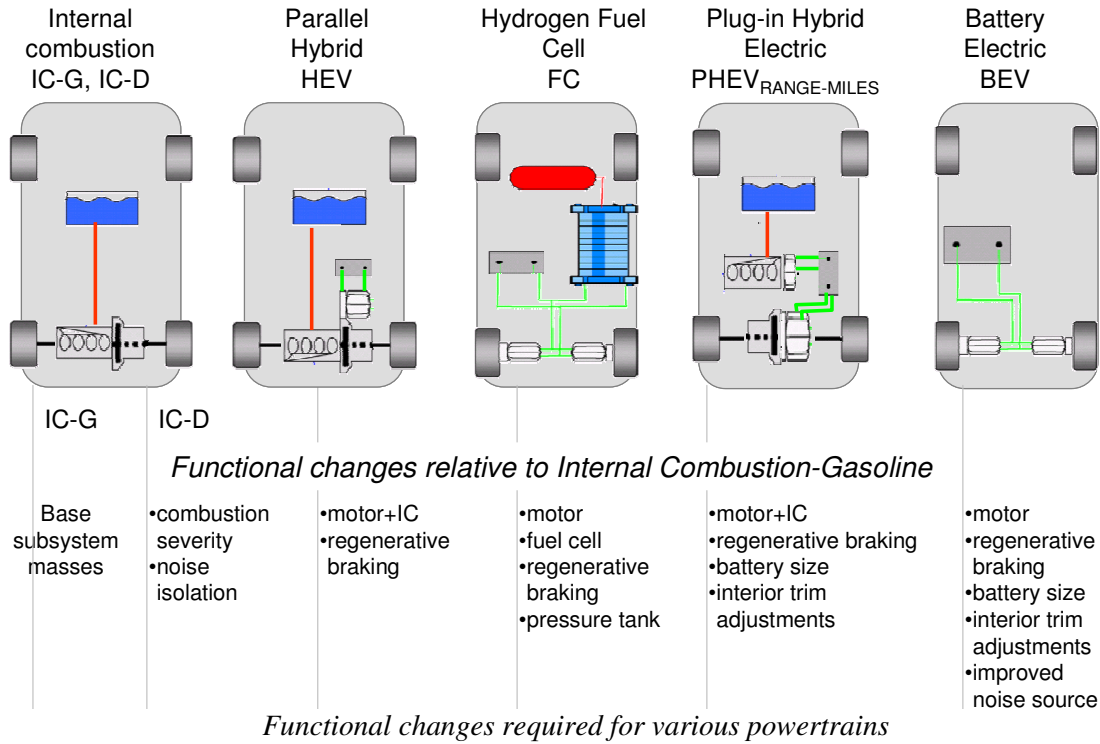
m_i = subsystem mass (kg)

m_{CURB} = curb mass (kg) for vehicle with specific powertrain $m_{CURB} = \sum m_i$

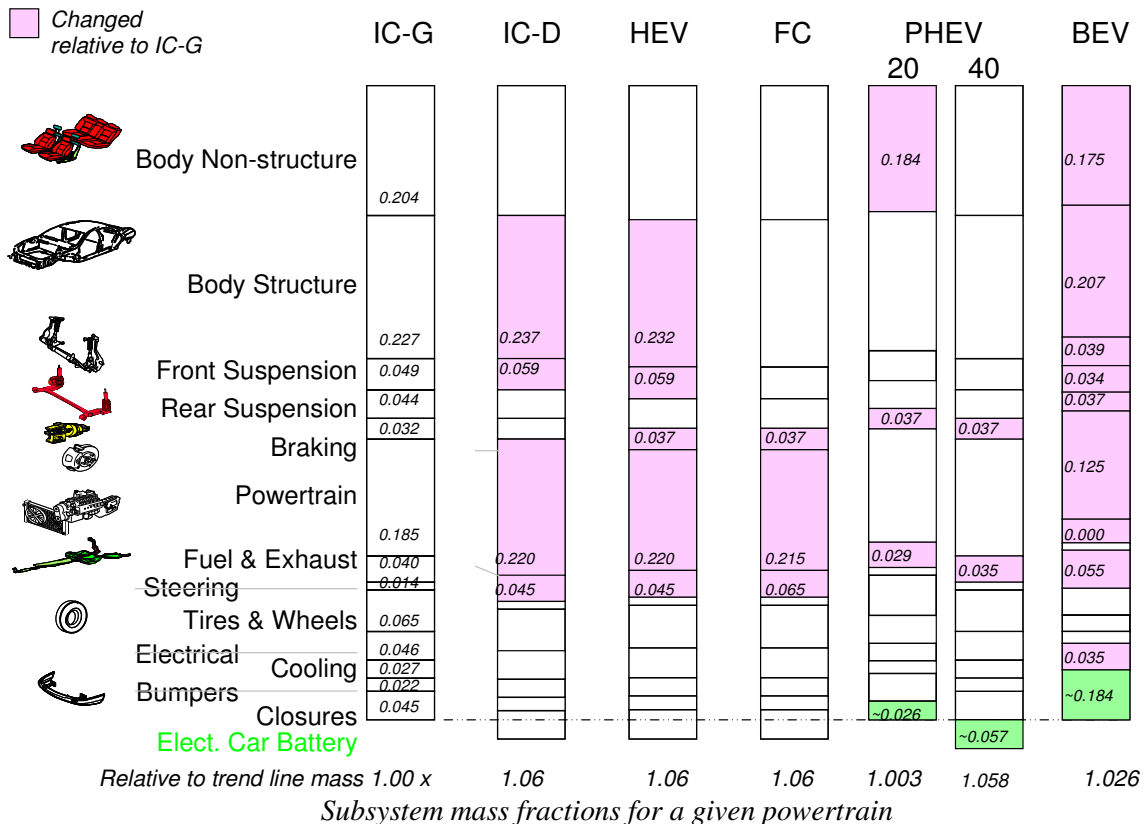
Data to evaluate the subsystem mass fraction were obtained from vehicle teardowns [1]. The illustration below shows subsystem mass data for several vehicles (sedan/hatchback FWD, integral body, gasoline internal combustion engines). The average values for each subsystem was used to estimate the mass fraction, ϕ_i , for the reference IC-gasoline case.



To evaluate the mass fractions for other powertrain types, the functional changes needed to replace a IC-gasoline with the alternative powertrain were considered, see illustration below. These functional changes then lead to changes in subsystems and a resulting change in subsystem mass fraction.



Based on these functional changes, the subsystem mass fractions are adjusted depending on the powertrain selected, illustration below.



The electric car battery sizing model is shown below and depends on frontal area, range, and curb mass [10]. Once the required battery power is determined, the battery mass is determined using energy density for a particular battery technology.

Power required

$$P_{BATTERY} = 0.0623 A_f \cdot R \cdot M_{CURB}$$

$P_{BATTERY}$ = required battery power (Wh)

A_f = vehicle frontal area (m^2)

R = range with fully charged battery (km)

M_{CURB} = vehicle curb mass (kg)

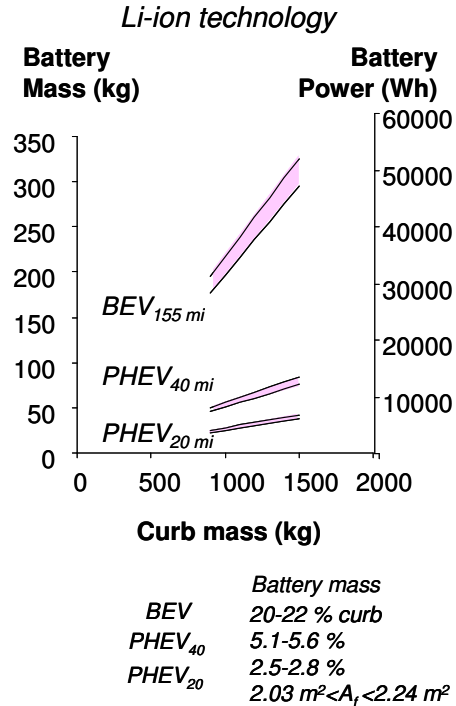
Battery Mass

$$m_{BATTERY} = \frac{P_{BATTERY}}{e_{DENSITY}}$$

$m_{BATTERY}$ = battery mass (kg)

$e_{DENSITY}$ = battery energy density (Wh/kg)

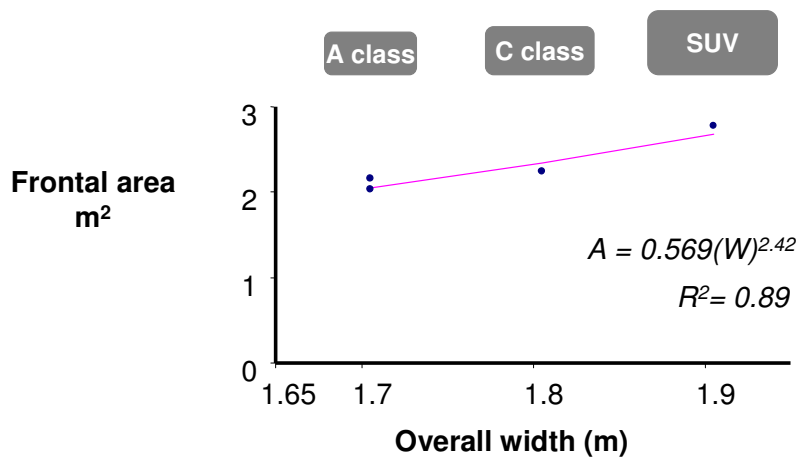
for Li-ion technology, $e_{DENSITY} = 155 \text{ Wh/kg}$



User Guide for Version 3 of the WorldAutoSteel Energy and GHG Model, Roland Geyer, WorldAutoSteel, 1/6/2011, page 24.

Battery Sizing Model

To implement this model, the vehicle frontal area is required. As this parameter is often unknown in the early design stage, overall width was used as an estimator for frontal area, see illustration below.



Estimating frontal area using overall width

3.1.1 Vehicle Bill of Material and Material Mass- To capture the material use in the vehicle, the Bill of Materials—BOM—is used. This is a matrix with each element being the fraction of a particular subsystem composed of a particular material,

$$\text{BOM} \quad \bar{\alpha} = \begin{bmatrix} \alpha_{11} & \alpha_{12} & \dots \\ \alpha_{21} & \alpha_{ij} & \dots \\ \dots & \dots & \dots \end{bmatrix}$$

where

α_{ij} =fraction of subsystem i composed of material j

Note that rows will sum to 1

$$\text{Subsystem mass vector} \quad \bar{m} = \begin{bmatrix} m_1 \\ m_i \\ \dots \end{bmatrix}$$

where

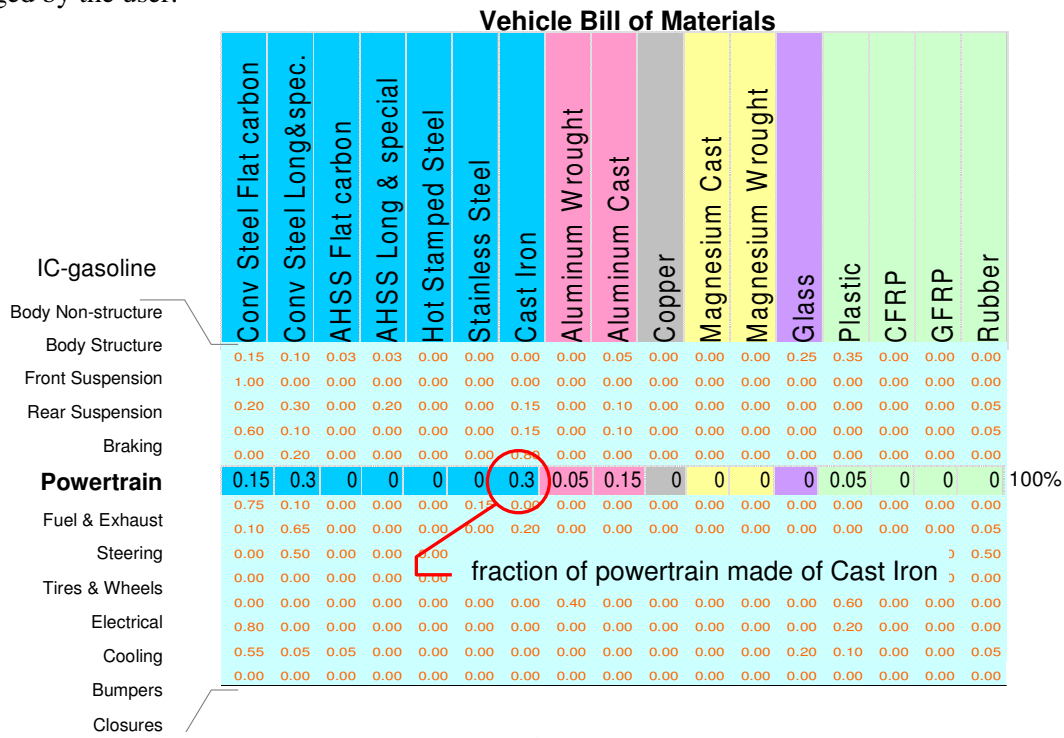
m_i =mass of subsystem i

$$\text{Total mass of material } j \text{ in vehicle} \quad \bar{m} = [m_1 \quad m_j \quad \dots] = [m_1 \quad m_i \quad \dots] \begin{bmatrix} \alpha_{11} & \alpha_{12} & \dots \\ \alpha_{21} & \alpha_{ij} & \dots \\ \dots & \dots & \dots \end{bmatrix} = (\bar{m})^T (\bar{\alpha})$$

where

m_j =total mass of material j in vehicle

The *Design Advisor* is pre-loaded with a conventional BOM resulting in 67% Ferrous material, 7% Aluminum, 5% Copper, 6% glass, 11% Plastics, 4% Rubber, and <1% other. This default may be changed by the user.



3.2 Scaling Component Mass - In general, the component data input has been sized for a specific vehicle. Attributes of the nominal vehicle may be different than this, and the component should be resized based on its specific mass driver. As an example, benchmark data for hood mass can be expressed as,

$$\hat{m}_{HOOD}(kg) = 11.06(Area \ m^2)^{0.867}$$

In this expression, the hood mass depends on hood Area—a mass driver for the hood. If we have mass data for a hood B with area $1.0 \ m^2$, we can scale that hood to estimate the mass of hood A with area $1.5m^2$,

$$m_A = m_B \left(\frac{1.5 \ m^2}{1.0 \ m^2} \right)^{0.867}$$

or in general,

$$\frac{m_A}{m_B} = \left[\frac{MassDriver_A}{MassDriver_B} \right]^\beta$$

$$m_A = \left[\frac{MassDriver_A}{MassDriver_B} \right]^\beta m_B$$

where

m_A = mass of component A to be determined

m_B = mass of reference component B

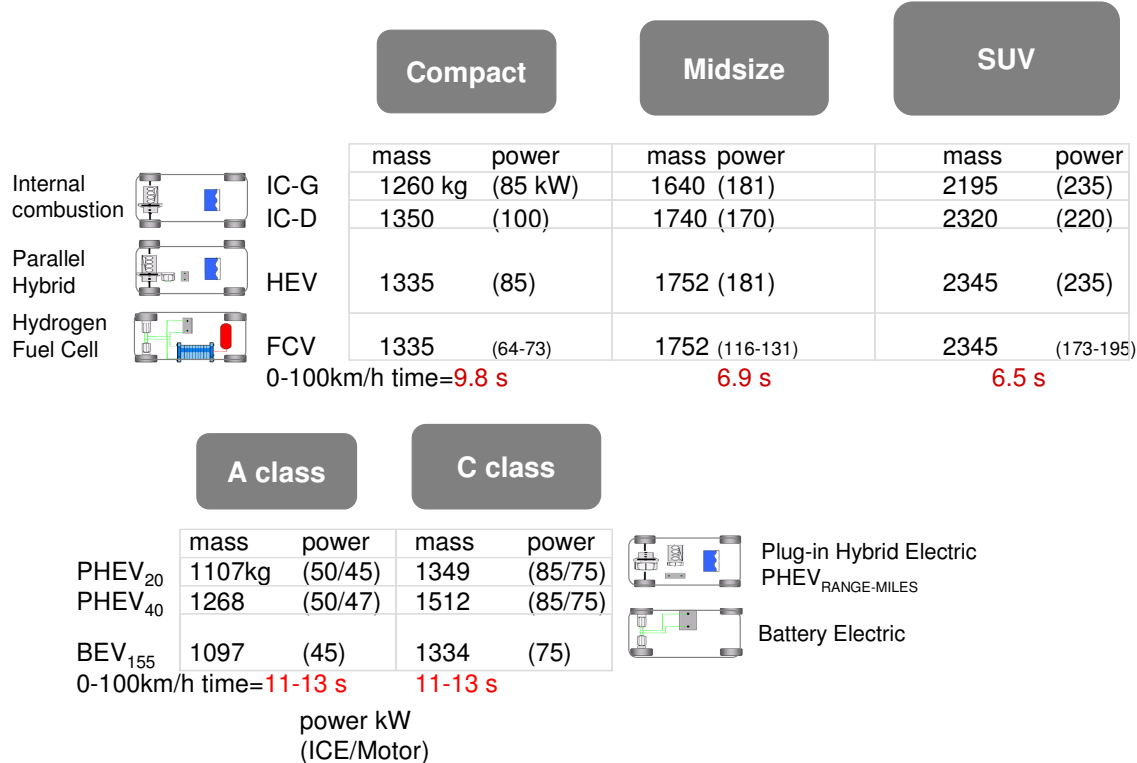
β = exponent for the significant mass driver

Mass drivers for components in the *Design Advisor* are summarized below.

Component name	Mass-Driver
Front Suspension Knuckle	Gross vehicle mass
Front Suspension lower control arm	Gross vehicle mass
Body Structure	Gross vehicle mass
Deck Lid Frame	Projected Area
Exhaust System	Engine displacement
Front Bumper Beam	Curb mass
Front Door Frame	Projected Area
Front Seat Frame	No mass driver
Front Suspension	Gross vehicle mass
Hatchback Frame	Projected Area
Hood Frame	Projected Area
Instrument Panel Beam	No mass driver
Lift Gate Frame	Projected Area
Other	User defined
Rear Bumper Beam	Curb mass
Rear Suspension	Gross vehicle mass
Wheels	Swept volume (circular area x width)

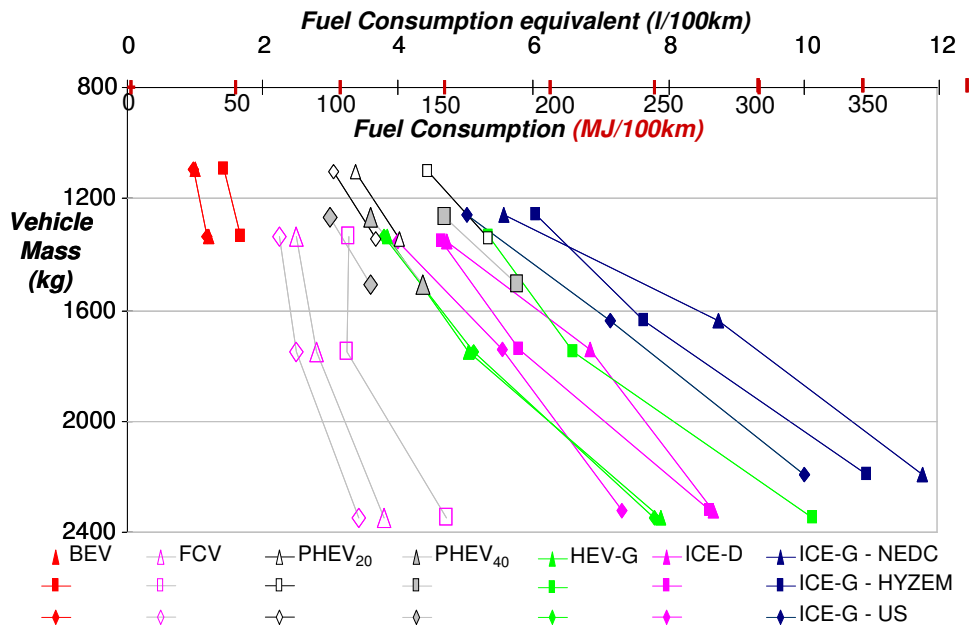
Mass Drivers

3.3 Powertrain Sizing for the Nominal Vehicle-To determine fuel consumption (energy demand), simulations were done for the 18 vehicles shown below[5, 6, 7, 17].



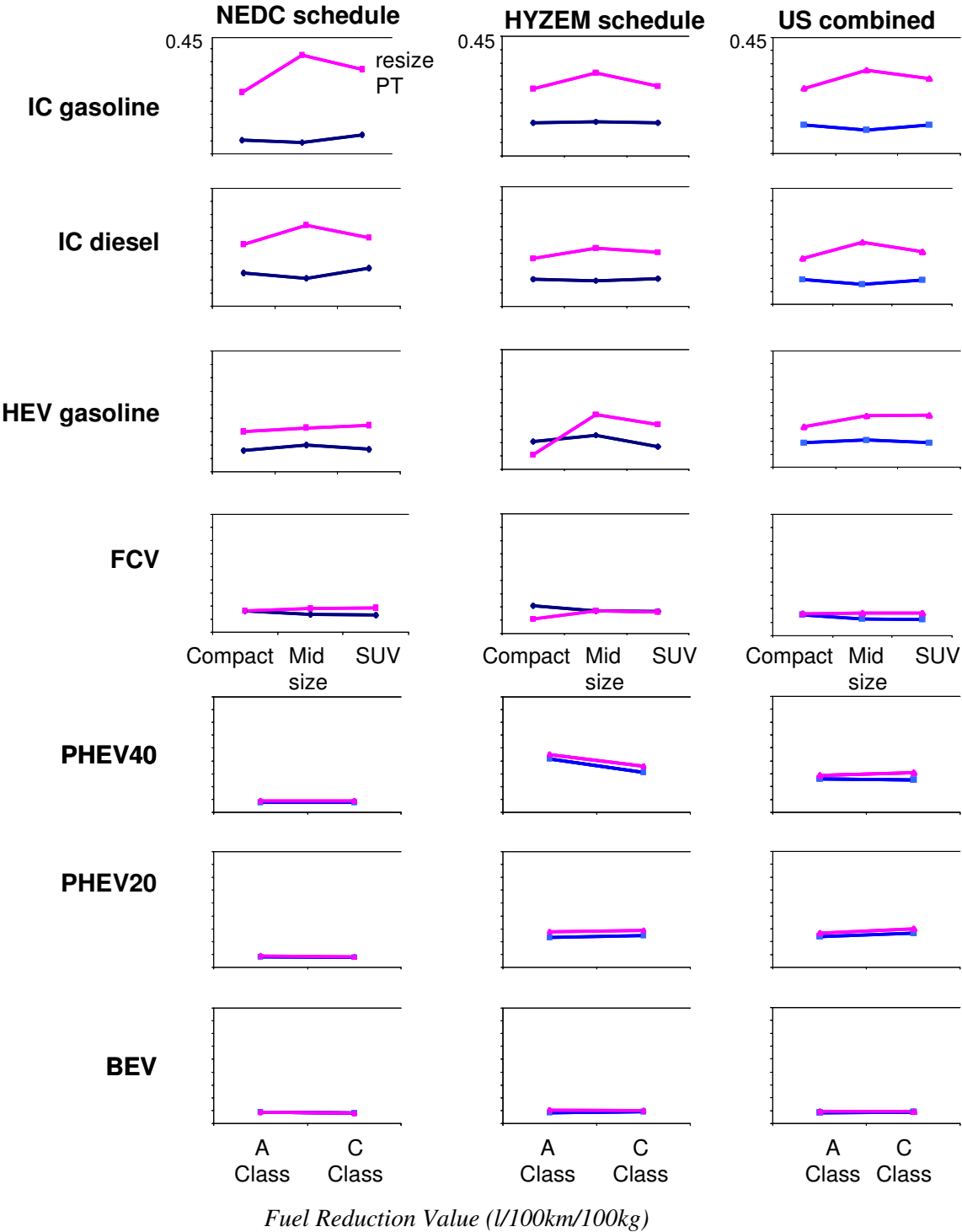
Vehicles Simulated [5, 6, 7, 17]

The resulting fuel consumption (energy demand) is summarized on the chart below. This data is used to estimate the fuel consumption of the nominal vehicle.



Energy Demand as a functional of vehicle mass

To estimate how fuel consumption changes due to mass reduction, a fuel consumption mass reduction value is applied. This value is defined as the reduction in energy consumption ($MJ/100\text{ km}$) per 100 kg of vehicle mass reduction. In the thumbnail graphs below, the fuel reduction value, FRV, is expressed in equivalent liters gasoline rather than energy. Note that the FRV is greatest for pure internal combustion powertrains, and is largest when the powertrain is resized—red line at top of each graph—to achieve constant acceleration performance (rather than keeping the same displacement—blue lines at bottom of each graph).



Using the energy demand and the Fuel Reduction Value, the calculation methodology to determine vehicle fuel consumption for the nominal and resized vehicles is as follows,

Calculation steps

- 1. set nominal vehicle mass
- 2. select powertrain technology
- 3. select fuel consumption schedule
- 4. select a consistent base fuel consumption (energy demand)

Example values

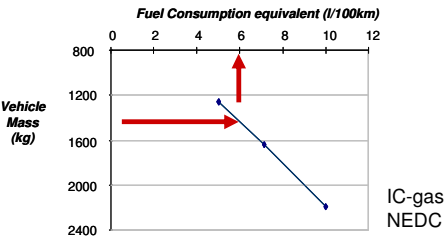
1400 kg



IC-g

NEDC

using energy demand graphs



6 l/100km

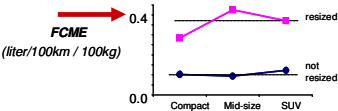
- 5. resize nominal vehicle for component mass change

1410 kg

- 6. calculate change in vehicle mass between nominal and resized, ΔM

10 kg

- 7. use FRV to determine change in fuel consumption $\Delta fuel consumption = FRV * \Delta M$



$$\Delta fc = (0.4 \text{ L}/100\text{km}/100\text{kg}) 10 \text{ kg} = 0.04 \text{ L}/100\text{km}$$

$$\text{resized fuel consumption} = 6 + 0.04 = 6.04 \text{ L}/100\text{km}$$

Fuel consumption calculation steps

3.4 Mass Estimation of the Resized Vehicle (mass compounding)- When the mass of a component is changed during vehicle design, other subsystems are also affected.. This effect is known as the secondary mass effect, and is captured in the following equations. For the overall vehicle mass,

$$M_{RS} = M_0 + \Delta + \Delta\Gamma$$

M_0 =Initial vehicle mass for which the subsystems are sized

Δ =Initial total mass change (primary mass change)

M_{RS} =Resized vehicle mass

$\Delta\Gamma$ =Additional (secondary) mass change due to resizing all subsystems

$$\Gamma = \gamma_V \quad \text{for simple secondary mass}$$

$$\Gamma = \frac{\gamma_V}{1 - \gamma_V} \quad \text{for compounded secondary mass}$$

γ_V =Mass influence coefficient for the vehicle given by $\gamma_V = \sum \gamma_i$

γ_i =Mass influence coefficient for subsystem i

The resulting mass for subsystem i due to an initial increase of Δ ;

$$mi_{RS} = mi_0 + \Delta_i + \Delta\tau$$

$$\tau = \gamma_i \quad \text{for simple secondary mass}$$

$$\tau = \frac{\gamma_i}{1 - \gamma_V} \quad \text{for compounded secondary mass}$$

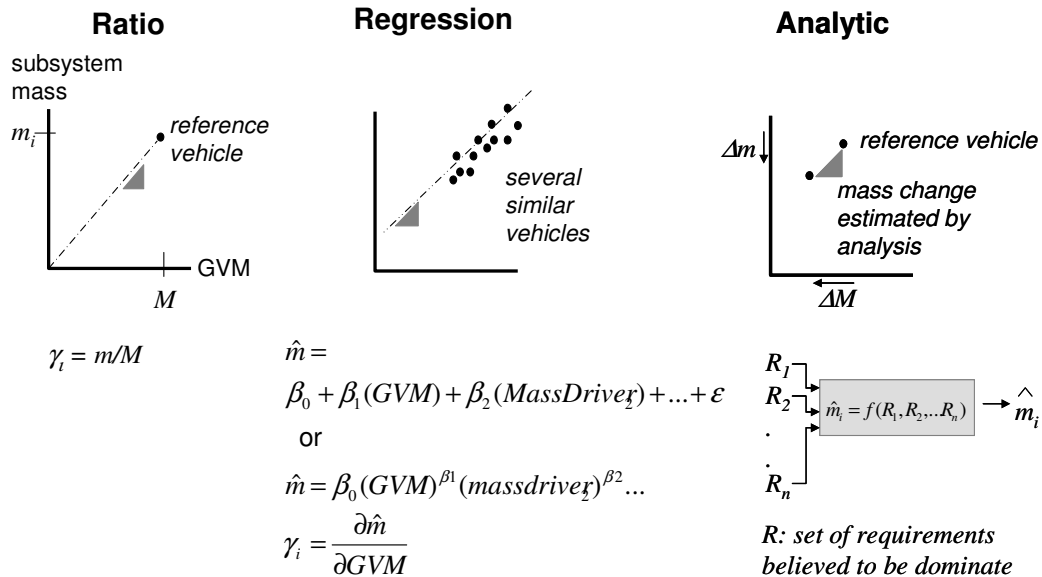
mi_0 =Initial subsystem i mass

Δ_i =Initial mass change in subsystem i

mi_{RS} =Resized subsystem i mass

$\Delta_i \tau$ =Additional (secondary) mass change for subsystem i

Three methods to estimate mass influence coefficients are shown below. The *Design Advisor* allows the user to select the method and to select simple or compounded mass.



Methods to estimate secondary mass influence coefficients

3.5 Primary Cost Estimation- The primary cost change is limited here to material cost and tooling and equipment cost for the primary shaping process. This is modeled by the following equation,

$$C = \left[\frac{m C_M}{1-f} \right] + \left[\frac{(C_T)}{n} \right] + \frac{1}{\dot{n}} \left(\frac{C_C}{L \cdot t_{WO}} \right) + \frac{1}{\dot{n}} \dot{C}_{OH}$$

- C =Cost per part (\$)
 C_M =Cost of material (\$/kg)
 f =Scrap fraction *note: (yield=1-f)*
 C_C =Cost of equipment (\$)
 C_T =Cost of tooling (\$)
 \dot{n} =Production rate (number of units made per year)
 n =Batch size
 m =Part mass (kg)
 t_{WO} =Capital write-off time (years equipment will be productive)
 L =Load factor (fraction of time equipment is productive)
 C_{OH} =Overhead rate (\$/yr)
 (all other costs of production not allocated directly to part)
 $C_{OH}=0$ for this analysis

Tooling cost and equipment cost are taken as dependent on part mass. For example, for steel the expressions are shown below.

Process	$\hat{Y} = \beta_0 (Mass)^{\beta_1} + \beta_2$
Equipment Cost	
Steel Stamping	$\hat{Y} = 2478928(Mass^{0.2282})(0.6494^{Shallow})(1.2202^{DeepDraw})$
Hot Stamping	$\hat{Y} = 2478928(Mass^{0.2282})(0.6494^{Shallow})(1.2202^{DeepDraw}) + 1.0E06$
Tailor Welded Blank Stamping	$\hat{Y} = 2478928(Mass^{0.2282})(0.6494^{Shallow})(1.2202^{DeepDraw}) + 3.8E06$
Non Ferrous Stamping	$\hat{Y} = 3167177(Mass^{0.2282})(0.6494^{Shallow})(1.2202^{DeepDraw})$
Tooling Cost	
Steel Stamping	$\hat{Y} = 506037(Mass^{0.402})(0.5081^{Shallow})(1.2643^{DeepDraw})$
Hot Stamping	$\hat{Y} = 506037(Mass^{0.402})(0.5081^{Shallow})(1.2643^{DeepDraw}) + 1.0E06$
Tailor Welded Blank Stamping	$\hat{Y} = 506037(Mass^{0.402})(0.5081^{Shallow})(1.2643^{DeepDraw}) + 3.8E06$
Non Ferrous Stamping	$\hat{Y} = 779106(Mass^{0.402})(0.5081^{Shallow})(1.2643^{DeepDraw})$

Example relationships to determine equipment and tooling cost as a function of part mass

The parameters used for tooling and equipment costs, material utilization and production rate, and material costs are found in the Appendix.

3.6 Subsystem Resizing Cost Estimation-When changing a component, other subsystems of the vehicle may be resized due to mass compounding. This causes a subsystem resizing cost,

$$\text{subsystem cost change} = (\text{subsystem mass change})(\text{subsystem cost/unit subsystem mass})$$

The subsystem cost/unit mass is determined by the material cost for the subsystem given by the following expressions.

Vehicle Bill of Material,

$$\bar{\alpha} = \begin{bmatrix} \alpha_{11} & \alpha_{12} & \dots \\ \alpha_{21} & \alpha_{22} & \dots \\ \dots & \dots & \dots \end{bmatrix}$$

where

α_{ij} =fraction of subsystem i composed of material j

Note that rows will sum to 1

Vector of material costs

$$\bar{c} = \begin{bmatrix} c_1 \\ c_j \\ \dots \end{bmatrix}$$

where

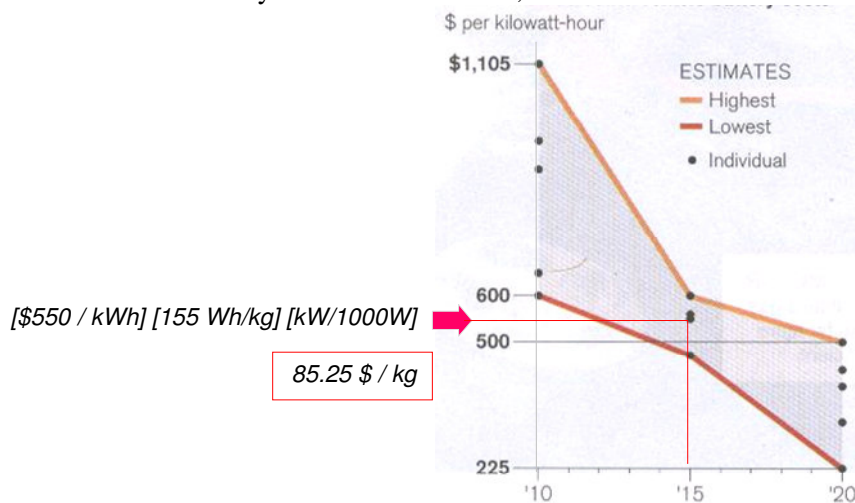
c_j =cost per unit mass of material j (\$/kg)

$$\text{Material cost of subsystem } i \text{ in vehicle } \bar{C}_i = \begin{bmatrix} C_1 \\ \dots \\ C_i \end{bmatrix} = \begin{bmatrix} \alpha_{11} & \alpha_{12} & \dots \\ \alpha_{21} & \alpha_{22} & \dots \\ \dots & \dots & \dots \end{bmatrix} \begin{bmatrix} c_1 \\ c_j \\ \dots \end{bmatrix} = (\bar{\alpha})(\bar{c})$$

where

C_i =total material cost of subsystem i in vehicle

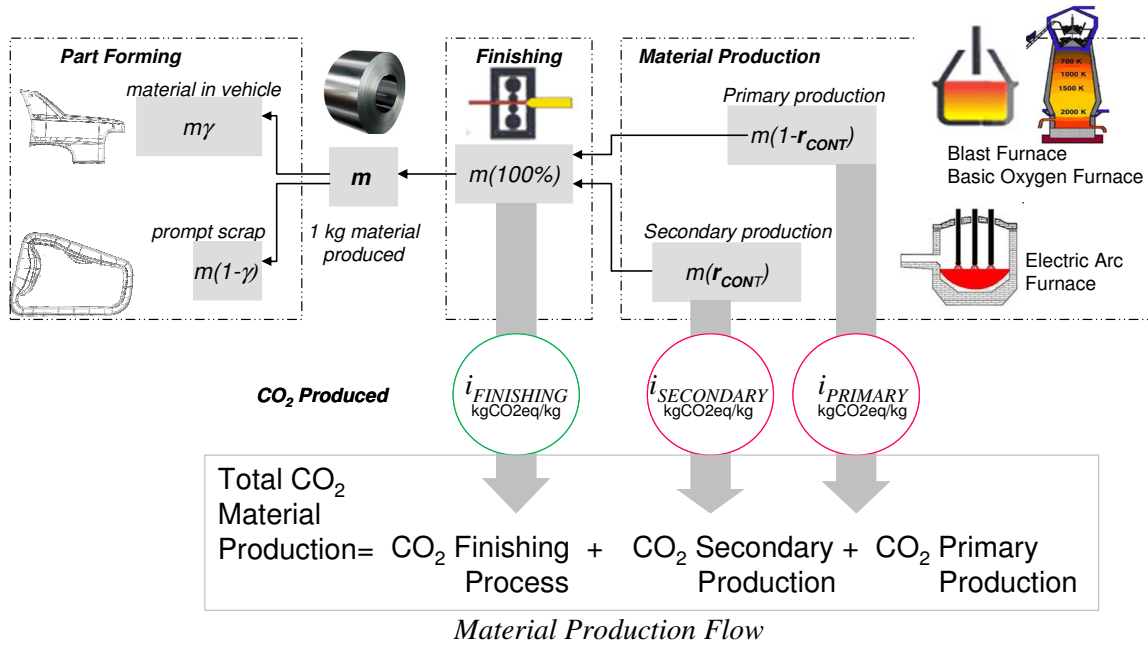
The electric car battery cost was taken to be,



Sources: Advanced Automotive Batteries, Boston Consulting Group, Deutsche Bank, Electrification Coalition, National Research Council, and Pike Research

Battery Cost

3.7 Life Cycle Assessment: Material Production- A typical material production sequence is shown below. Material is produced by both a primary production process using basic ore, and also a secondary process using recycled material. After production, the material enters a finishing process (cold rolling in this example) resulting in one unit of material entering the vehicle manufacturing process. Green house gas is produced in the finishing, secondary, and primary production steps. The greenhouse gas calculation is indicated below.



Total CO₂ Material Production =

$$[CO_2 \text{ Primary Production}] + [CO_2 \text{ Secondary Production}] + [CO_2 \text{ Finishing Process}]$$

$$I_{MAT} = [m(1 - r_{CONT})i_{PRIMARY}] + [mr_{CONT}i_{SECONDARY}] + [mi_{FINISHING}]$$

$$I_{MAT} = m[(1 - r_{CONT})i_{PRIMARY} + r_{CONT}i_{SECONDARY} + i_{FINISHING}]$$

$$I_{MAT} = m[i_{TOTAL_PRODUCTION}]$$

Where

m = mass of material produced

I_{MAT} = CO₂ resulting from production of m kg of finished material (kg CO₂eq)

r_{CONT} = fraction of material from secondary production

$i_{PRIMARY}$ = CO₂ resulting from primary production of 1 kg (kg CO₂eq/kg material)

$i_{SECONDARY}$ = CO₂ resulting from secondary production of 1 kg (kg CO₂eq/kg material)

$i_{FINISHING}$ = CO₂ resulting from finishing process of 1 kg (kg CO₂eq/kg material)

$i_{TOTAL_PRODUCTION}$ = CO₂ resulting from complete production of 1 kg (kg CO₂eq/kg material)
(resource extraction (cradle) to factory gate)

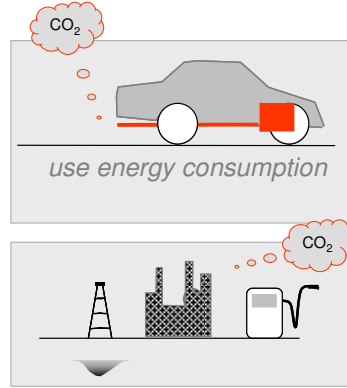
Part shaping process GHG $I_{SHAPE} = m i_{SHAPE}$

Where

m = Mass of material to shaping process (kg)

i_{SHAPE} = CO₂/kg material

3.8 Life Cycle Assessment: Use Phase- Greenhouse gas produced during the use phase falls in two areas, the GHG due to fuel consumed in using the vehicle (tank to wheels), and the GHG due to producing the fuel (wheel to tank). Both sources are accounted for in the Design Advisor using the following expressions.



Use phase GHG areas

$$I_{USE} = I_{WELL_TANK} + I_{TANK_WHEELS}$$

$$I_{WELL_TANK} = [i_{FUEL_PRODUCTION}] R_L (ED)$$

$$I_{TANK_WHEELS} = [i_{FUEL_COMBUSTION}] R_L (ED)$$

Where

ED = Energy demand per unit distance (MJ/100km)

$ED_{NOMINAL\ VEHICLE}$ = f(vehicle mass, schedule) from fka simulations

$ED_{RESIZED\ VEHICLE} = (ED)_{NOM} + (\Delta m)(FCME)$

(Δm) = Difference in mass between resized and nominal vehicles (kg)

$(FCME)$ = Fuel Consumption mass elasticity (MJ/100kg)

R_L = life time range (km)

I_{USE} = CO₂ resulting from vehicle use over life (kg CO₂eq)

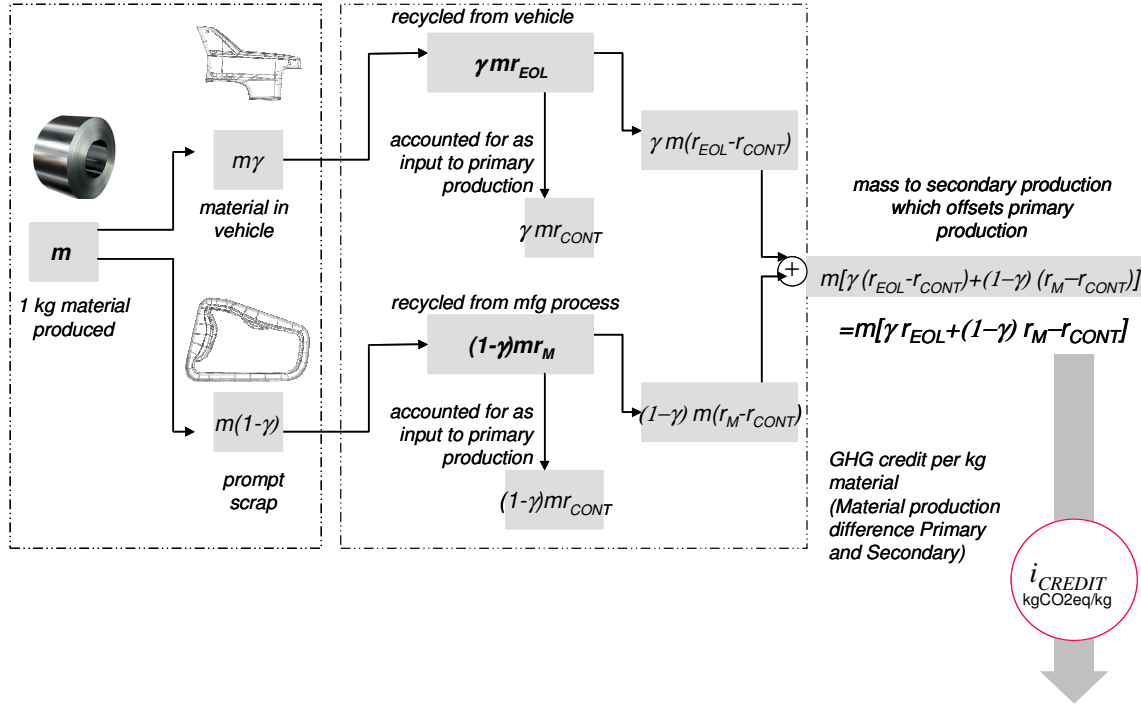
$i_{FUEL_PRODUCTION}$ = CO₂ resulting from production of 1 unit of fuel (kg CO₂eq/MJ)

$i_{FUEL_COMBUSTION}$ = CO₂ resulting from combustion of 1 unit of fuel (kg CO₂eq/MJ)

note: Gasoline equivalent energy demand (liter/100km) = ED / Q_{LHV}

Q_{LHV} = Lower Heating Value of fuel (MJ/liter) (for gasoline Q_{LHV} = 31.88 MJ/liter)

3.9 Life Cycle Assessment: Recycle- The flow of a unit of material is shown below at the end-of-life stage. A greenhouse gas credit results by displacing a unit of primary material production with a unit of secondary production.



Material Recycling Flow

$$I_{RECYCLE} = (1-\alpha)m[\gamma(r_{EOL}-r_{CONT})+(1-\gamma)(r_M-r_{CONT})](i_{SECONDARY}-i_{PRIMARY})$$

Where

m = mass of material produced (kg)

$I_{RECYCLE}$ = CO₂ credit from end of life of (mγ) kg of material from vehicle (kg CO₂eq)

r_M = Prompt scrap recycling rate

r_{EOL} = End of Life recycle rate for vehicle

r_{CONT} = Scrap input to primary production

γ = Vehicle production forming yield (from material mass of m, part mass of mγ results)

i_{CREDIT} = GHG credit per kg material (Material production difference between Secondary and Primary)

$i_{PRIMARY}$ = Environmental impact of primary material production

$i_{SECONDARY}$ = Environmental impact of secondary material production

$(1-\alpha)$ = Factor for Consequential System Expansion method

References

1. A2mac1.com Automotive benchmarking, Ypsilanti, MI.
2. Anderson, M., *Course notes for Global Vehicle Integration*, AUTO 501, University of Michigan, 2010.
3. CES EduPack 2012 Version 11.9.9, Grant Design Limited, www.grantadesign.com, Cambridge, UK.
4. EDAG, *WorldAutoSteel - Future Steel Vehicle Phase 2—Report*, April 20, 2011.
5. fka, Wohlecker, Roland, et al., *Determination of Weight Elasticity of Fuel Economy for Conventional ICE Vehicles, Hybrid Vehicles and Fuel Cell Vehicles*, fka, Report 55510, June 2007.
6. fka, Schulte-Corne, Claus, et al., *Determination of weight influence on the energy consumption of battery electric vehicles and plugin hybrid vehicles*, fka, Report 99280, January, 2010.
7. fka, Schulte-Corne, Claus, et al., *Determination of weight influence on the energy consumption according to US regulations*, fka, Report 105620, April 2011.
8. Fuchs, Hannes, *A/SP Lightweight Suspension Front Lower Control Arm Design Optimization*, Great Designs in Steel Seminar, 2010.
9. Geyer, R., *Life Cycle Greenhouse Gas Emission Assessments of Automotive Materials, Methodology Report*, UCSB, WorldAutoSteel, December, 2007
10. Geyer, R., *User Guide for Version 3 of the WorldAutoSteel Energy and GHG Model*, UCSB, WorldAutoSteel, January 6, 2012.
11. Malen D. & Reddy, K., *Preliminary Vehicle Mass Estimation Using Empirical Subsystem Influence Coefficients*, Auto/Steel Partnership, June 26, 2007
12. Malen D., *Automotive Mass Benchmarking*, Auto/Steel Partnership and USAMP, May 15, 2010
13. <http://www.epa.gov/nvfel/testing/dynamometer.htm> , US Driving Schedules, US EPA.
14. <http://www.epa.gov/otaq/tcldata.htm>, Test car data files, US EPA.
15. <http://greet.es.anl.gov/main>, *Greenhouse Gases, Regulated Emissions, and Energy Use in Transportation*, Argonne Nat. Lab, US DOE.
16. USLAB-AVC, *Engineering Report*, Porsche Engineering Services, Oct, 2001, Chapter 15: CO₂ and vehicle performance.
17. fka, Scholz-Starke, et al, *Determination of Weight Influence on Energy Consumption under EPA Conditions*, Report 124960, November 2012.

Appendix A. Notation

A_f	Vehicle frontal area (m^2)
c_j	Cost per unit mass of material j (\$/kg)
L_i	Total material cost of subsystem i in vehicle (\$)
C	Cost per part (\$)
C_C	Cost of equipment (\$)
C_M	Cost of material (\$/kg)
C_{OH}	Overhead rate (\$/yr)
C_T	Cost of tooling (\$)
$e_{DENSITY}$	Battery energy density (Wh/kg)
ED	Energy demand (MJ/100km)
(FCME)	Fuel Consumption mass elasticity (MJ/100kg)
f	Scrap fraction note: (yield=1-f)
i	Subscript for subsystem
$i_{FUEL_PRODUCTION}$	GHG resulting from production of 1 unit of fuel (kg CO ₂ eq/MJ)
$i_{FUEL_COMBUSTION}$	GHG resulting from combustion of 1 unit of fuel (kg CO ₂ eq/MJ)
i_{CREDIT}	GHG credit per kg material (Material production difference between Secondary and Primary)
$i_{PRIMARY}$	GHG for primary material production per unit mass (kg CO ₂ eq/kg)
$i_{SECONDARY}$	GHG for secondary material production per unit mass (kg CO ₂ eq/kg)
I_-	GHG total (kg CO ₂ eq), subscript for USE, MATERIAL PRODUCTION, RECYCLE
j	Subscript for material
L	Vehicle length (m)
L	Load factor (fraction of time equipment is productive)
m_{CURB}	Curb mass (kg)
m_i	Subsystem mass (kg)
m_j	total mass of material j in vehicle
m_{i_0}	Initial subsystem i mass
$m_{i_{RS}}$	Resized subsystem i mass
M_0	Initial vehicle mass for which the subsystems are sized
M_{RS}	Resized vehicle mass
\dot{n}	Production rate (number of units made per year)
n	Batch size (number of parts made over life of design)
m	Part mass (kg)
$P_{BATTERY}$	Required battery power (Wh)
r_M	Prompt scrap recycling rate
r_{EOL}	End of Life recycle rate for vehicle
r_{CONT}	Scrap input to primary production
R	Range with fully charged battery (km)
R_L	Life time range (km)
T_{WO}	Capital write-off time (years equipment will be productive)
Q_{LHV}	Lower Heating Value of fuel (MJ/liter) (for gasoline $Q_{LHV}=31.88$ MJ/liter)
W	Vehicle width
α_{ij}	fraction of subsystem i composed of material j
β	Regression coefficient
Δ	Initial total mass change (primary mass change)
Δ_i	Initial mass change in subsystem i
(Δm)	Difference in mass between resized and nominal vehicles (kg)
ϕ_i	Mass fraction relative to curb mass for subsystem i
γ	Forming yield (from material mass of m, part mass of $m\gamma$ results)
γ_i	Mass influence coefficient for subsystem i

Appendix B. Parameters loaded in spreadsheets

Input Component Data Sheet

Table of vehicle subsystems
B59:B71

Body Non-structure
Body Structure
Front Suspension
Rear Suspension
Braking
Powertrain
Fuel & Exhaust
Steering
Tires & Wheels
Electrical
Cooling
Bumpers
Closures

Table of Part materials
B93:B104

Steel-Conventional
Steel-AHSS
Steel-Hot Stamped
Steel-Stainless
Cast Iron
Aluminum Wrought
Aluminum Cast
Magnesium Wrought
Magnesium Cast
CFRP
GFRP
SMC

Table of Part shaping processes
G94:G106

Steel Stamping
Steel Tailor Welded Blank Stamping
Steel Hot Stamping
Steel Open Roll Form
Steel Tubular Hydroforming
Steel Forging
Iron Casting
NonFerrous Stamping
NonFerrous Extrusion
NonFerrous Die Casting
NonFerrous Forging
Composite Sheet Molding Compound
Composite Resin Transfer

Table of benchmarked components and mapping:

Component to vehicle subsystem, mass driver, units, scaling exponent, and mass benchmark equation
G59:P74

Body Structure	Body Structure	GVM	kg	0.44	Picture 6695
Front Door Frame	Closures	Door Area	m ²	0.87	Picture 6680
Hood Frame	Closures	Hood Area	m ²	1.24	Picture 6681
Deck Lid Frame	Closures	Deck Lid Area	m ²	1.18	Picture 6682
Hatchback Frame	Closures	Hatchback Area	m ²	0.55	Picture 6683
Lift Gate Frame	Closures	Liftgate Area	m ²	0.44	Picture 6684
Instrument Panel Beam	Body Structure	No mass driver		1.00	Picture 6691
Front Bumper Beam	Bumpers	Curb Mass	kg	0.55	Picture 6692
Rear Bumper Beam	Bumpers	Curb Mass	kg	0.87	Picture 6693
Front Seat Frame	Body Non-structure	No mass driver		1.00	Picture 6690
Front Suspension Knuckle	Front Suspension	GVM	kg	0.48	Picture 6686
Front Suspension Lower Control Arm-McPherson	Front Suspension	GVM	kg	0.90	Picture 6687
Front Suspension Lower Control Arm-SLA	Front Suspension	GVM	kg	1.04	Picture 6687
Wheels	Tires & Wheels	Swept Volume	mm ³	0.63	Picture 6689
Exhaust System	Fuel & Exhaust	Engine Disp.	liter	1.00	Picture 6694
Other	N/A	No mass driver		1.00	Picture 6792

Input Component Data Sheet-continued

Table of compatible materials and processes
G130:R135

Steel-Conventional	Steel-AHSS	Steel-Hot Stamped	Steel-Stainless	Cast Iron
Steel Stamping	Steel Stamping	Steel Hot Stamping	Steel Stamping	Iron Casting
Steel Tailor Welded Blank Stamping	Steel Tailor Welded Blank Stamping		Steel Tailor Welded Blank Stamping	
Steel Open Roll Form	Steel Open Roll Form		Steel Open Roll Form	
Steel Tubular Hydroforming	Steel Tubular Hydroforming		Steel Tubular Hydroforming	
Steel Forging	Steel Forging		Steel Forging	

Table continued

Aluminum Wrought	Aluminum Cast	Magnesium Wrought	Magnesium Cast	CFRP	GFRP	SMC
NonFerrous Stamping	NonFerrous Die Casting	NonFerrous Stamping	NonFerrous Die Casting	Composite Sheet Molding Compound	Composite Sheet Molding Compound	Composite Sheet Molding Compound
NonFerrous Extrusion		NonFerrous Extrusion		Composite Resin Transfer	Composite Resin Transfer	
NonFerrous Forging		NonFerrous Forging				

Set Nominal Vehicle Sheet

Table of subsystem mass fractions for various powertrain selections

A51:L66

Sub-system	IC-gasoline	IC-diesel	Parallel hybrid-gasoline	Fuel Cell	Plug in Hybrid-20 mile range	Plug in Hybrid-40 mile range	Battery Electric-140 mile range	
1	0.204	0.204	0.204	0.204	0.184	0.204	0.175	Body Non-structure
2	0.227	0.237	0.232	0.227	0.227	0.227	0.207	Body Structure
3	0.049	0.059	0.059	0.049	0.049	0.049	0.039	Front Suspension
4	0.044	0.044	0.044	0.044	0.044	0.044	0.034	Rear Suspension
5	0.032	0.032	0.037	0.037	0.037	0.037	0.037	Braking
6	0.185	0.220	0.220	0.215	0.185	0.185	0.109	Powertrain
7	0.040	0.045	0.045	0.065	0.029	0.035	0.000	Fuel & Exhaust
8	0.014	0.014	0.014	0.014	0.014	0.014	0.014	Steering
9	0.065	0.065	0.065	0.065	0.065	0.065	0.055	Tires & Wheels
10	0.046	0.046	0.046	0.046	0.046	0.046	0.046	Electrical
11	0.027	0.027	0.027	0.027	0.027	0.027	0.027	Cooling
12	0.022	0.022	0.022	0.022	0.022	0.022	0.022	Bumpers
13	0.045	0.045	0.045	0.045	0.045	0.045	0.035	Closures
14					0.029 Depends on curb mass	0.058 Depends on curb mass	0.226 Depends on curb mass	Battery (electric car)
total	1.000	1.060	1.060	1.060	1.003	1.058	1.026	

Table for curb mass estimate for Nominal gasoline IC vehicle

B67:E70

Vehicle Type	Slope: Curb Mass to Area (kg/m ²)	Intercept: Curb Mass to Area Intercept (kg)	standard error (kg)
Sedan/Hatchback	169.71	0.00	132.00
SUV	229.00	0.00	132.00
User Defined	0	0	0

Set Nominal Vehicle Sheet –continued

Table for default material mass fractions for each subsystem and materials in the vehicle Bill of Materials
N73:AF86

	Conv Steel Flat carbon	Conv Steel Long&spec.	AHSS Flat carbon	AHSS Long & special	Hot Stamped Steel	Stainless Steel	Cast Iron	Aluminum Wrought	Aluminum Cast	Copper	Magnesium Cast	Magnesium Wrought	Glass	Plastic	CFRP	GFRP	Rubber	Battery (electric car)	other (no GHG)
Body Non-struct	0.15	0.1	0.03	0.03	0	0	0	0	0.1	0	0	0	0.3	0.4	0	0	0	0	0.1
Body Struct	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Front Susp	0.2	0.3	0	0.2	0	0	0.15	0	0.1	0	0	0	0	0	0	0	0.1	0	0
Rear Susp	0.6	0.1	0	0	0	0	0.15	0	0.1	0	0	0	0	0	0	0	0.1	0	0
Brake		0.2	0	0	0	0	0.8	0	0	0	0	0	0	0	0	0	0	0	0
Pwrtrn	0.15	0.3	0	0	0	0	0.3	0.1	0.2	0	0	0	0	0.1	0	0	0	0	0
Fuel & Exh	0.75	0.1	0	0	0	0.15	0	0	0	0	0	0	0	0	0	0	0	0	0
Steer	0.1	0.65	0	0	0	0	0.2	0	0	0	0	0	0	0	0	0	0.1	0	0
Tires & Wheel	0	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0	0
Elect	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
Cool	0	0	0	0	0	0	0	0.4	0	0	0	0	0	0.6	0	0	0	0	0
Bmpr	0.8	0.0	0.0	0.0	0.0	0	0	0	0	0	0	0	0	0.2	0	0	0	0	0
Clsure	0.55	0.05	0.05	0.0	0.0	0	0	0	0	0	0	0	0.2	0.1	0	0	0.1	0	0
Battry elcCar	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0

Table for electric car range

D73:G79

Internal Combustion-gasoline	0
Internal Combustion-diesel	0
Parallel hybrid-gasoline	0
Fuel Cell	0
Plug in Hybrid-20 mile range	20
Plug in Hybrid-40 mile range	40
Battery Electric- 155 mile range	155

Battery energy density

D89

Battery energy density	Wh/kg	155
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Battery cost /kWh

D98

Battery cost projected 2015	\$/kWh	550
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Component Mass Benchmarking Sheet

Table of benchmark data for all components

P53:CH179

Refer to Excel sheet

List of component mass equations

A73:A145

Refer to Excel sheet

Powertrain Sizing Sheet

Table of compatible powertrains and fuels

J85:P91

Internal Combustion- gasoline	Internal Combustion-diesel	Parallel hybrid- gasoline	Fuel Cell	Plug in Hybrid-20 mile range	Plug in Hybrid-40 mile range	Battery Electric- 140 mile range
Gasoline	Diesel	Gasoline	Hydrogen	Electricity- USA	Electricity- USA	Electricity- USA
E85	BioDiesel	E85		Electricity- Europe	Electricity- Europe	Electricity- Europe
				Electricity- China	Electricity- China	Electricity- China
				Electricity- Japan	Electricity- Japan	Electricity- Japan
				Electricity- India	Electricity- India	Electricity- India
				Electricity- Coal	Electricity- Coal	Electricity- Coal

Table of energy demands for various powertrains and vehicle mass

E219:M280

Refer to Excel sheet

Mass Compounding sheet

Table of secondary mass coefficients

D53:J68

sub-system	not used	Analytical	Regression	Ratio	User Defined	
1		0.0000	0.0000	(varies with specific case)		Body Non-structure
2		0.0961	0.1267			Body Structure
3		0.0248	0.0272			Front Suspension
4		0.0248	0.0276			Rear Suspension
5		0.0367	0.0238			Braking
6		0.0813	0.0929			Powertrain
7		0.0101	0.0607			Fuel & Exhaust
8		0.0070	0.0086			Steering
9		0.0218	0.0497			Tires & Wheels
10		0.0000	0.0000			Electrical
11		0.0000	0.0000			Cooling
12		0.0000	0.0347			Bumpers
13		0.0000	0.0000			Closures
14		0.0000	0.0000			Battery (electric car)
Sum		0.3025	0.4519			

Component Cost Sheet

Table of material cost for component
B176:C188

Material	Typical \$/kg
Steel-Conventional	0.7025
Steel-AHSS	0.9550
Steel-Hot Stamped	1.4800
Steel-Stainless	1.8970
Cast Iron	0.5975
Aluminum Wrought	2.4650
Aluminum Cast	2.5600
Magnesium Wrought	4.9350
Magnesium Cast	4.9950
CFRP	42.1500
GFRP	20.4000
SMC	5.6250

Table of coefficients for equipment and tool cost
E174:O188

Process	tool	tool	tool	tool	tool	equipment	equipment	equipment	equipment	equipment
	param 1	param 2	param 3	opt 1	opt 2	param 1	param 2	param 3	Opti 1	opt 2
Steel Stamping	506037	0.402		0.5081	1.2643	2478928	0.2282		0.6494	1.2202
Steel Tailor Welded Blank Stamping	506037	0.402		0.5081	1.2643	2478928	0.2282	3800000	0.6494	1.2202
Steel Hot Stamping	506037	0.402		0.5081	1.2643	2478928	0.2282	1000000	0.6494	1.2202
Steel Open Roll Form	230.6	1	4897	1	1	6573.1	1	245343	1	1
Steel Tubular Hydroforming	-	1	690000	1	1		1	3350000	1	1
Steel Forging	947.46	1	7530.5	1	1	47206	1	376528	1	1
Iron Casting	0.3931	1	942.8	1	1	6.2836	1	18897	1	1
NonFerrous Stamping	779106	0.402		0.5081	1.2643	3167177	0.2282		0.6494	1.2202
NonFerrous Extrusion	314.18	1	939.86	1	1	141868	1	187581	1	1
NonFerrous Die Casting	9551.3	1	8384.5	1	1	62886	1	188371	1	1
NonFerrous Forging	3158.2	1	7530.5	1	1	157353	1	376528	1	1
Composite Sheet Molding Compound	2994.3	1	9340.2	1	1	8337.5	1	65750	1	1
Composite Resin Transfer	57.459	1	897.03	1	1	958.74	1	8663	1	1

$$\text{Cost} = (\text{Param 1})(\text{part mass, kg})^{\text{Param 2}} [(\text{OPT1})^{\text{SHALLOW}} (\text{OPT2})^{\text{DEEP}}] + (\text{Param 3})$$

Where

The bracketed term is used only for stamping

SHALLOW=1 if selected, 0 otherwise

DEEP=1 if selected, 0 otherwise

Component Cost Sheet –continued

Equipment and tool cost equations dependent on coefficients

Process	
Equipment Cost	
Steel Stamping	$\hat{Y} = 2478928(Mass^{0.2282})(0.6494^{Shallow})(1.2202^{DeepDraw})$
Hot Stamping	$\hat{Y} = 2478928(Mass^{0.2282})(0.6494^{Shallow})(1.2202^{DeepDraw}) + 1.0E06$
Tailor Welded Blank Stamping	$\hat{Y} = 2478928(Mass^{0.2282})(0.6494^{Shallow})(1.2202^{DeepDraw}) + 3.8E06$
Non Ferrous Stamping	$\hat{Y} = 3167177(Mass^{0.2282})(0.6494^{Shallow})(1.2202^{DeepDraw})$
Tooling Cost	
Steel Stamping	$\hat{Y} = 506037(Mass^{0.402})(0.5081^{Shallow})(1.2643^{DeepDraw})$
Hot Stamping	$\hat{Y} = 506037(Mass^{0.402})(0.5081^{Shallow})(1.2643^{DeepDraw}) + 1.0E06$
Tailor Welded Blank Stamping	$\hat{Y} = 506037(Mass^{0.402})(0.5081^{Shallow})(1.2643^{DeepDraw}) + 3.8E06$
Non Ferrous Stamping	$\hat{Y} = 779106(Mass^{0.402})(0.5081^{Shallow})(1.2643^{DeepDraw})$

Tubular Hydroforming	
Equipment Cost	$\hat{Y} = 3.35E06$
Tooling Cost	$\hat{Y} = 6.90E05$

Process	Equipment Cost	Tooling Cost
Steel Open Roll Form	$\hat{Y} = 6573.1(Mass) + 245343$	$\hat{Y} = 230.6(Mass) + 4897$
Steel Forging	$\hat{Y} = 47206(Mass) + 376528$	$\hat{Y} = 947.46(Mass) + 7530.5$
Iron Casting	$\hat{Y} = 6.2836(Mass) + 18897$	$\hat{Y} = 0.3931(Mass) + 942.8$
Non Ferrous Extrusion	$\hat{Y} = 141868(Mass) + 187581$	$\hat{Y} = 314.18(Mass) + 939.86$
Non Ferrous Die Casting	$\hat{Y} = 62886(Mass) + 188371$	$\hat{Y} = 9551.3(Mass) + 8384.5$
Non Ferrous Forging	$\hat{Y} = 157353(Mass) + 376528$	$\hat{Y} = 3158.2(Mass) + 7530.5$
Sheet Molding Compound	$\hat{Y} = 8337.5(Mass) + 65750$	$\hat{Y} = 2994.3(Mass) + 9340.2$
Resin Transfer Method	$\hat{Y} = 958.74(Mass) + 8663$	$\hat{Y} = 57.459(Mass) + 897.03$

Subsystem Cost Sheet

Table of material cost for vehicle bill of materials
Y107:Z125

	Material price \$/kg
Conv Steel Flat carbon	0.7025
Conv Steel Long&spec.	0.9385
AHSS Flat carbon	0.948375
AHSS Long & special	1.266975
Hot Stamped Steel	1.48
Stainless Steel	1.89675
Cast Iron	0.5975
Aluminum Wrought	3.16125
Aluminum Cast	2.56
Copper	7.285
Magnesium Cast	4.935
Magnesium Wrought	4.935
Glass	6.14
Plastic	3
CFRP	42.15
GFRP	20.4
Rubber	3.96
Battery (electric car)	85.25

LCA Material Sheet

Table of material production parameters for GHG for vehicle Bill of Materials
B102:G119 (Reference UCSB Excel Model)

	Material Flows C97 Mat from secondary production, r_{CONT} %	Materials G93 (for conv steel) Emissions from primary production (kgCO ₂ eq/kg produced)	Materials G94 (for conv steel) Emissions from secondary production (kgCO ₂ eq/kg produced)	Materials G100 (for conv steel) Emissions from material finishing (kgCO ₂ eq/kg produced)	Material Flows K97 Forming Manufacturing yield γ (%)
Conv Steel Flat carbon	0.05	1.87	0.40	0.49	0.55
Conv Steel Long&spec.	0.85	1.87	0.40	0.29	0.75
AHSS Flat carbon	0.05	1.87	0.40	0.49	0.55
AHSS Long & special	0.85	1.87	0.40	0.29	0.75
Hot Stamped Steel	0.05	1.87	0.40	0.49	0.55
Stainless Steel	0.05	1.87	0.40	0.49	0.55
Cast Iron	1.00	1.87	0.40	0.14	0.80
Aluminum Wrought	0.00	10.51	0.69	0.87	0.66
Aluminum Cast	0.85	10.51	0.69	0.62	0.80
Copper	0.00	3.74	0.00	0.00	1.00
Magnesium Cast	0.00	35.10	21.00	21.00	0.55
Mag Wrought	0.00	35.10	0.80	0.80	0.96
Glass	0.00	1.07	0.00	0.00	1.00
Plastic	0.00	3.62	0.00	0.00	0.90
CFRP	0.00	22.00	0.00	0.00	0.50
GFRP	0.00	8.00	0.00	0.00	0.50
Rubber	0.00	2.90	0.00	0.00	0.90
Battery (electric car)	0.00	18.60	0.00	0.00	1.00

Table of material production and shaping process GHG parameters for Part
B136:G148

	Mat from secondary production, r_{CONT} %	Emissions from primary production (kgCO ₂ eq/kg produced)	Emissions from secondary production (kgCO ₂ eq /kg produced)	Emissions from material finishing (kgCO ₂ eq /kg produced)	Forming Manufacturing yield γ (%)
Steel-Conventional	0.05	1.87	0.40	0.49	0.55
Steel-AHSS	0.05	1.87	0.40	0.49	0.55
Steel-Hot Stamped	0.05	1.87	0.40	0.49	0.55
Steel-Stainless	0.05	1.87	0.40	0.49	0.55
Cast Iron	1.00	1.87	0.40	0.14	0.80
Aluminum Wrought	0.00	10.51	0.69	0.87	0.66
Aluminum Cast	0.85	10.51	0.69	0.62	0.80
Mag Wrought	0.00	35.10	0.80	0.80	0.96
Magnesium Cast	0.00	35.10	21.00	21.00	0.55
CFRP	0.00	22.00	0.00	0.00	0.50
GFRP	0.00	8.00	0.00	0.00	0.50
SMC	0.00	8.00	0.00	0.00	0.50

LCA Material Sheet-continuedTable of Shaping Process GHG kg CO2/kg
I136:U148

	Steel Stamp	Steel Tailor Welded Blank Stamp	Steel Hot Stamp	Steel Open Roll Form	Steel Tubular Hydro forming	Steel Forging	Iron Casting	Non Ferrous Stamp	Non Ferrous Extrusion	Non Ferrous Die Casting	Non Ferrous Forging	Composite Sheet MoldComp	Composite Resin Trans
Steel-Conv	0.203	0.203		0.203	0.203	0.203							
Steel-AHSS	0.271	0.271		0.271	0.271	0.271							
Steel-Hot Stamp			0.675										
Steel-Stainless	0.271	0.271		0.271	0.271								
Cast Iron							0.797						
Alum Wrght								0.505	0.987		0.6766		
Alum Cast										0.835			
Mag Wrght								0.457	0.924		0.6766		
Mag Cast										0.823			
CFRP												0.28	0.28
GFRP												0.28	0.28
SMC												0.28	

LCA-Use Sheet

Table of fuel properties

C83:J97

	Fuel production	Fuel production	Fuel combustion	Combustion	fuel cost
	Fuel E30 (for Gas) Energy demand	Fuel G30 (for Gas) GHG	Fuel G73 (for Gas) GHG	Fuel D92 (for Gas) Energy liquid MJ/liter	
	MJ/MJ	(gm CO2eq/MJ)	(gm CO2eq/MJ)		\$/L,\$/kwhr
Gasoline	0.21	17.97	71.90	31.88	0.97
Diesel	0.14	12.10	76.30	35.95	1.04
E85-corn	0.65	64.57	15.13	22.72	0.95
BioDiesel-soybeans	0.27	49.00	0.00	32.64	1.00
Hydrogen	0.77	132.00	0.00	31.88	
Electricity-USA	2.64	208.50	0.00	1.00	0.10
Electricity-Europe	2.26	144.53	0.00	1.00	0.20
Electricity-China	2.86	270.28	0.00	1.00	0.15
Electricity-Japan	2.40	165.75	0.00	1.00	0.25
Electricity-India	2.85	256.39	0.00	1.00	0.10
Electricity-Coal	3.26	333.69	0.00	1.00	0.09

Table of fuel source by powertrain type

C113:G122

	Energy source for various powertrains		Data Input J126 percent driving mix-elect/fuel
	Liquid fuel	electricity	
Internal Combustion-gasoline	1	0	
Internal Combustion-diesel	1	0	
Parallel hybrid-gasoline	1	0	
Fuel Cell	1	0	
Plug in Hybrid-20 mile range	0.5	0.167	0.5 elect
Plug in Hybrid-40 mile range	0.5	0.167	0.5 elect
Battery Electric- 140 mile range	0	1	

LCA-Use Sheet-continued

Table of fuel consumption reduction for *liquid fuels same powertrain displacement*

I62:N71 (NEW ED-ES D18) Note: DA uses the same Fuel Consumption Reduction across all vehicle msss.

(MJ/100kg)	same powertrain displacement (inc perf)				
Powertrain from 'Set Nominal Vehicle' sheet list	HYZEM	NEDC	US Comb	US Highway	US City
Internal Combustion-gasoline	4.069	3.441	3.324	2.251932	4.849324
Internal Combustion-diesel	3.639	4.485	3.186	2.24369	4.567041
Parallel hybrid-gasoline	3.397	2.796	3.083	2.123464	3.859896
Fuel Cell	2.893	2.279	2.111	1.634325	2.537657
Plug in Hybrid-20 mile range	4.188	3.100	3.697		
Plug in Hybrid-40 mile range	3.886	4.437	4.306		
Battery Electric- 140 mile range	0.000	0.000	0.000		

Table of fuel consumption reduction for *liquid fuels powertrain displacement resized*

P62:T71 (NEW ED-ES D30)

(MJ/100kg)	HYZEM	NEDC	US Com	US Hiway	US City
Internal Combustion-gasoline	8.860	11.515	9.247	6.610483	12.97713
Internal Combustion-diesel	7.237	9.652	7.422	5.275385	10.40687
Parallel hybrid-gasoline	5.939	5.140	5.910	5.205484	6.480586
Fuel Cell	2.355	2.810	2.651	1.987078	3.241993
Plug in Hybrid-20 mile range	5.070	4.006	4.148		
Plug in Hybrid-40 mile range	5.291	5.376	5.106		
Battery Electric- 140 mile range	0.000	0.000	0.000		

Table of fuel consumption reduction for *electricity same powertrain displacement*

V62:Z71 (NEW ED-ES K18)

(MJ/100kg)	HYZEM	NEDC	US comb	US Hiway	US City
Internal Combustion-gasoline	0	0	0	0	0
Internal Combustion-diesel	0	0	0	0	0
Parallel hybrid-gasoline	0	0	0	0	0
Fuel Cell	0	0	0	0	0
Plug in Hybrid-20 mile range	1.42604	1.257063	1.35838	2.851586	4.96742
Plug in Hybrid-40 mile range	1.434639	1.269371	1.424193	2.517869	5.319639
Battery Electric- 140 mile range	1.41596	1.264472	1.448176	0.931794	1.704994

Table of fuel consumption reduction for *electricity powertrain displacement resized*

AB62:AF71 (NEW ED-ES K30)

(MJ/100kg)	HYZEM	NEDC	US Comb	US Hiway	US City
Internal Combustion-gasoline	0	0	0	0	0
Internal Combustion-diesel	0	0	0	0	0
Parallel hybrid-gasoline	0	0	0	0	0
Fuel Cell	0	0	0	0	0
Plug in Hybrid-20 mile range	1.615881	1.3808	1.460205	3.498146	5.286579
Plug in Hybrid-40 mile range	1.627076	1.386149	1.546266	3.549518	5.66624
Battery Electric-140 mi range	1.596435	1.293654	1.450687	1.122712	1.763017

LCA-Recycle Sheet

Table of parameters for GHG credit for materials in the vehicle Bill of Materials
D101:K119

	Material Flows K97 Forming Yield γ from LCA- Material sheet	Material Flows R97 Recycling rate matl in vehicle r_{EOL} %	Materials G95 (for conv steel) Emission credit (kgCO ₂ eq/kg recycled)	Material Flows N97 prompt scrap recycle rate R_M %	Material Flows C97 Mat from secondary production, r_{CONT} %	Material Flows D97 NOT USED S_P =scrap input to primary production	Data Input E135 alpha
Conv Steel Flat carbon	0.55	0.903	1.471	0.97	0.05	0.106	0.1
Conv Steel Long&spec.	0.75	0.903	1.471	0.97	0.85	0.106	0.1
AHSS Flat carbon	0.55	0.903	1.471	0.97	0.05	0.106	0.1
AHSS Long & special	0.75	0.903	1.471	0.97	0.85	0.106	0.1
Hot Stamped Steel	0.55	0.903	1.471	0.97	0.05	0.106	0.1
Stainless Steel	0.55	0.903	1.471	0.97	0.05	0.106	0.1
Cast Iron	0.80	0.903	1.471	0.97	1	0	0.1
Aluminum Wrought	0.66	0.786	9.82	0.921	0	0	0.1
Aluminum Cast	0.80	0.786	9.82	0.921	0.85	0	0.1
Copper	1.00	0.9	1	0	0	0	0.1
Magnesium Cast	0.55	0.786	31.5	0.921	0	0	0.1
Magnesium Wrought	0.96	0.786	31.5	0.921	0	0	0.1
Glass	1.00	0	0	0	0	0	0.1
Plastic	0.90	0.7	1	1	0	0	0.1
CFRP	0.50	0	22	0	0	0	0.1
GFRP	0.50	0	8	0	0	0	0.1
Rubber	0.90	0	0	0	0	0	0.1
Battery (electric car)	1.00	0	4.82	0	0	0	0.1

Table of parameters for GHG credit for materials in the part
D123:I135

	Forming Yield γ %	Recycling rate matl in vehicle reol %	Emission credit kg CO ₂ /kg	prompt scrap recycle rate R_M %	Mat from secondary production, r_{CONT} %
Steel-Conventional	0.55	0.90	1.47	0.97	0.05
Steel-AHSS	0.55	0.90	1.47	0.97	0.05
Steel-Hot Stamped	0.55	0.90	1.47	0.97	0.05
Steel-Stainless	0.55	0.90	1.47	0.97	0.05
Cast Iron	0.80	0.90	1.47	0.97	1.00
Alum Wrought	0.66	0.79	9.82	0.92	0.00
Aluminum Cast	0.80	0.79	9.82	0.92	0.85
Mag Wrought	0.96	0.79	31.50	0.92	0.00
Magnesium Cast	0.55	0.79	31.50	0.92	0.00
CFRP	0.50	0.00	22.00		0.00
GFRP	0.50	0.00	8.00		0.00
SMC	0.50	0.00	8.00		0.00